

Differential Kinematics

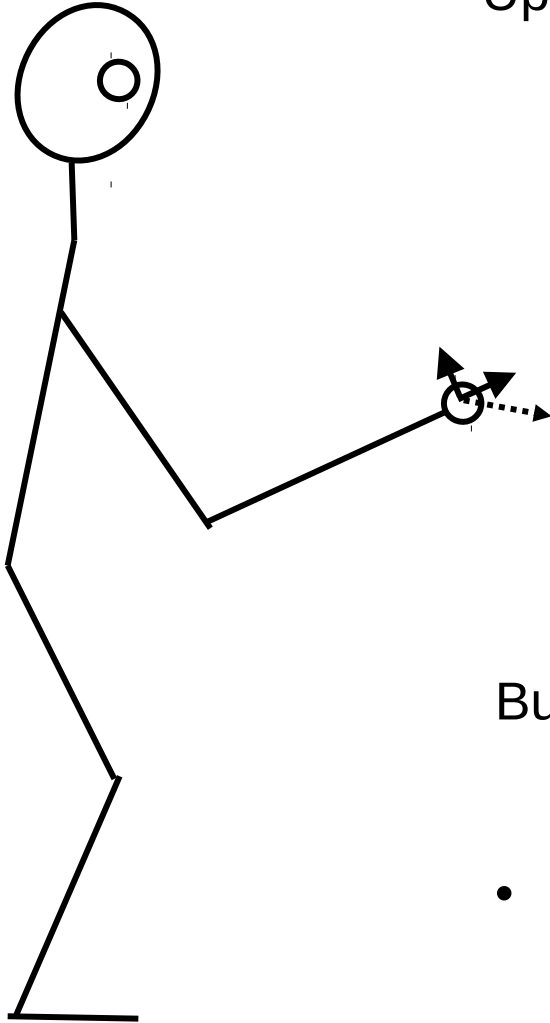
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Differential Kinematics

Up to this point, we have only considered the relationship of the joint angles to the Cartesian location of the end effector:

$$f(q) = x$$



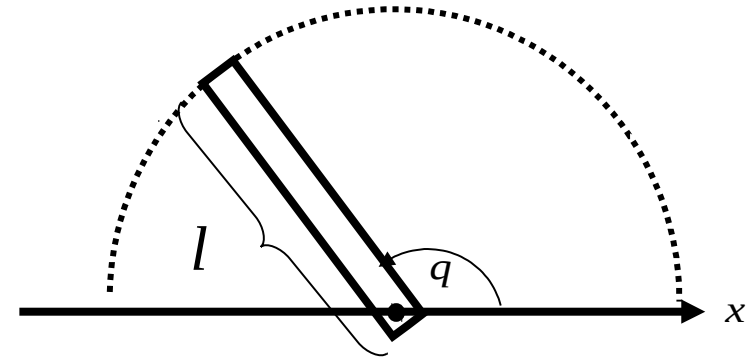
But what about the first derivative? $\frac{\partial f(q)}{\partial q}$

- This would tell us the velocity of the end effector as a function of joint angle velocities.

Motivating Example

Consider a one-link arm

- As the arm rotates, the end effector sweeps out an arc
- Let's assume that we are only interested in the x coordinate...



Forward kinematics: $x = l \cos(q)$

Differential kinematics: $\frac{dx}{dq} = -l \sin(q)$

$$\delta x = -l \sin(q) \delta q$$

$$\delta q = -\frac{1}{l \sin(q)} \delta x$$

Motivating Example

Suppose you want to move the end effector above a specified point, x_g

Answer #1: $q_g = \cos^{-1} \left(\frac{x_g}{l} \right)$

Answer #2: 1. $i = 0, q_0 = \text{arbitrary}$

2. $x_i = l \cos(q_i)$

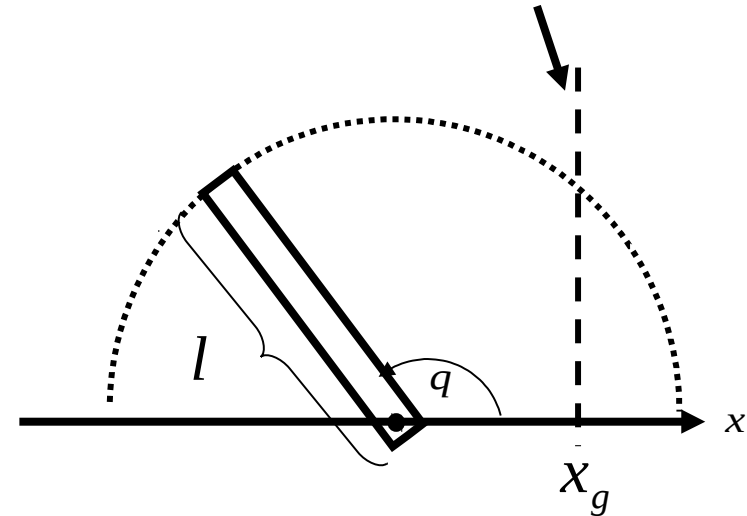
3. $\delta x = \alpha(x_g - x_i)$

4. $\delta q = \frac{1}{-l \sin(q_i)} \delta x$

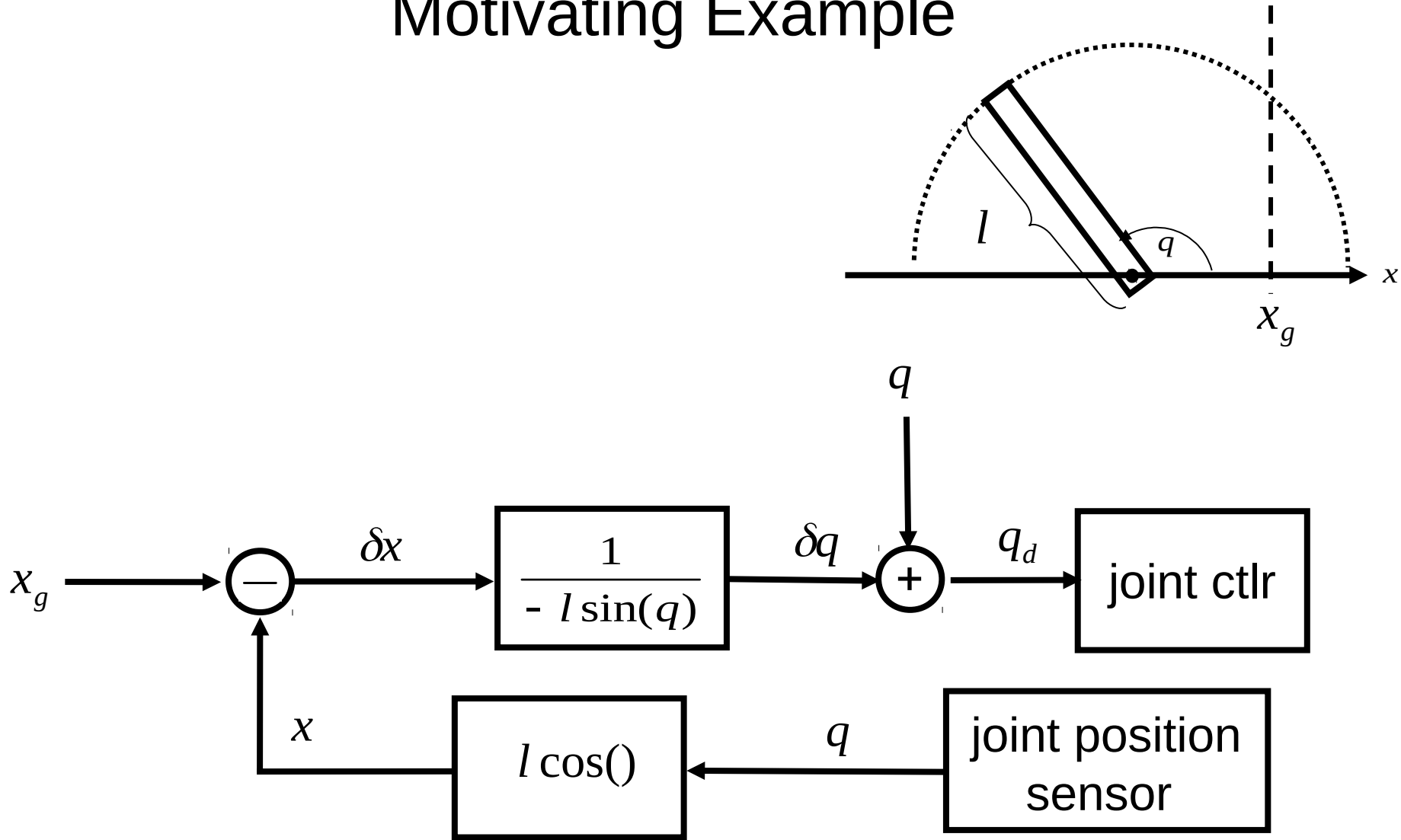
5. $q_{i+1} = q_i + \delta q$

6. $i++$ goto 2.

Goal: move the end effector onto this line



Motivating Example

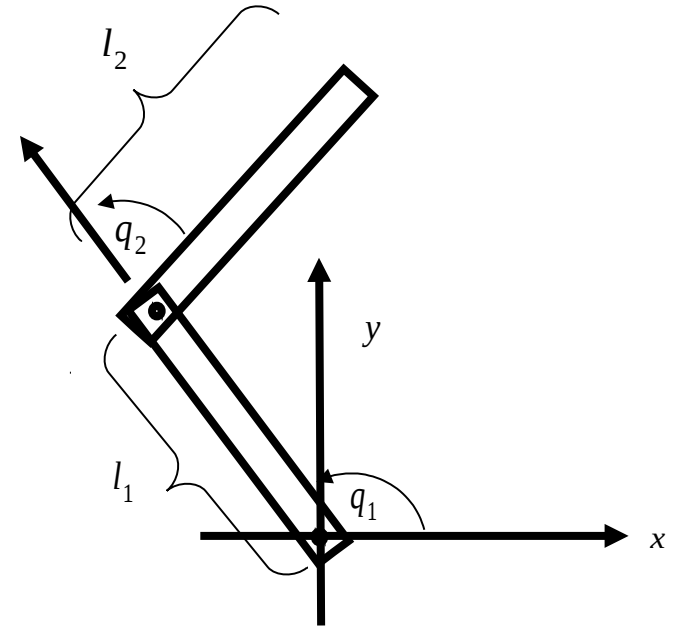


This controller moves the link asymptotically toward the goal position.

Intro to the Jacobian

$$\dot{x} = \begin{bmatrix} l_1 \cos(q_1) + l_2 \cos(q_1 + q_2) \\ l_1 \sin(q_1) + l_2 \sin(q_1 + q_2) \end{bmatrix}$$

Forward kinematics of the two-link manipulator



Velocity Jacobian



$$\frac{dx}{dq} = \begin{pmatrix} -l_1 \sin(q_1) - l_2 \sin(q_1 + q_2) & -l_2 \sin(q_1 + q_2) \\ l_1 \cos(q_1) + l_2 \cos(q_1 + q_2) & -l_2 \cos(q_1 + q_2) \end{pmatrix}$$

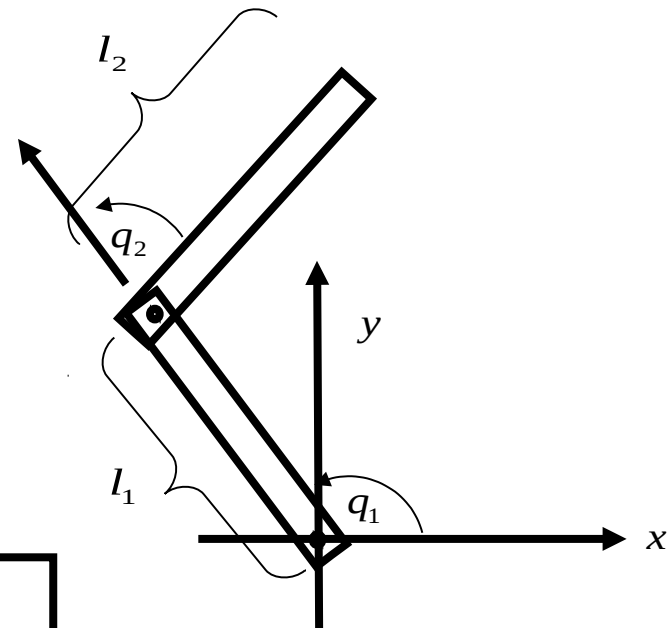
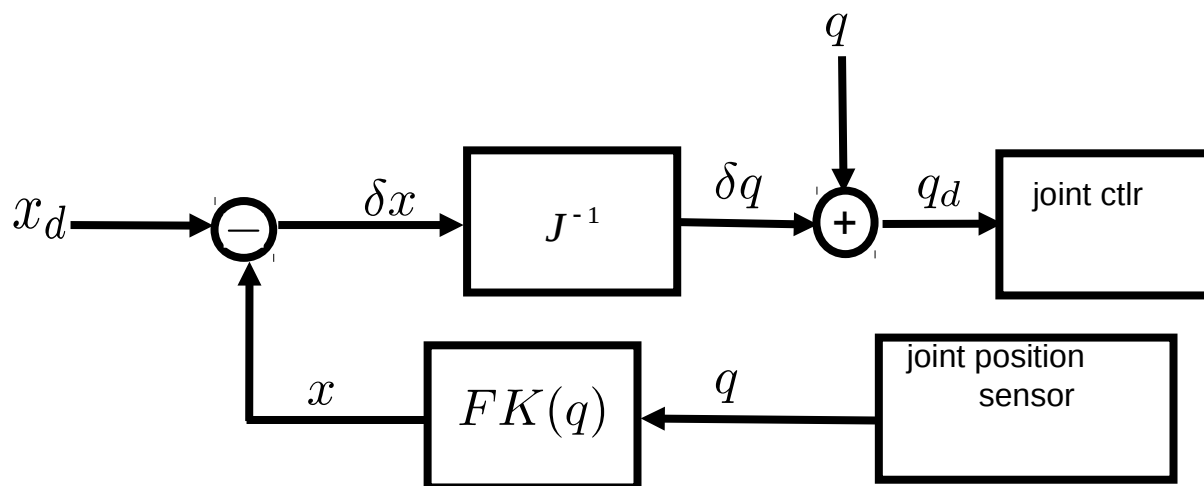
$$= J(q)$$

Intro to the Jacobian

$$J(q) = \begin{pmatrix} -l_1 \sin(q_1) - l_2 \sin(q_1 + q_2) & -l_2 \sin(q_1 + q_2) \\ l_1 \cos(q_1) + l_2 \cos(q_1 + q_2) & -l_2 \cos(q_1 + q_2) \end{pmatrix}$$

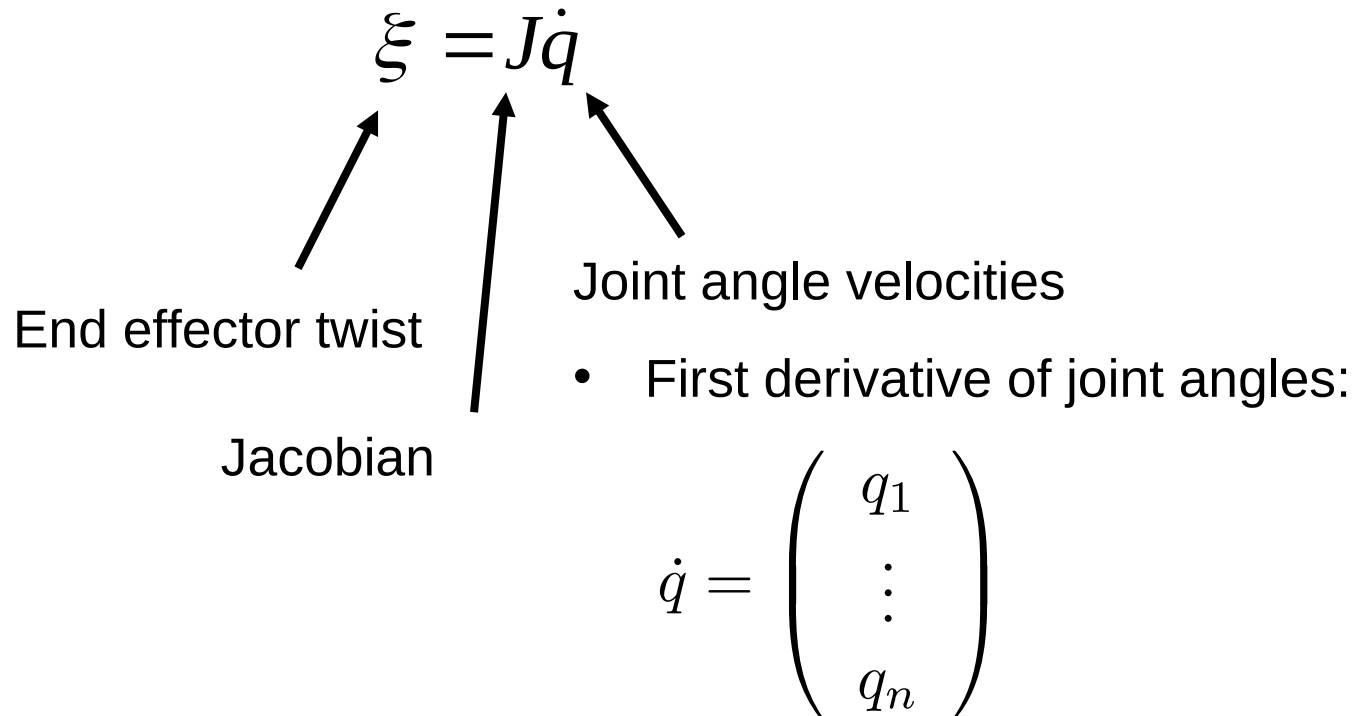
Chain rule: $\delta x = J \delta q$

If the Jacobian is square and full rank, then we can invert it: $\delta q = J^{-1} \delta x$



Jacobian

The Jacobian relates joint velocities with end effector *twist*:



It turns out that you can “easily” compute the Jacobian for arbitrary manipulator structures

- This makes differential kinematics a much easier sub-problem than kinematics in general.

What is Twist?

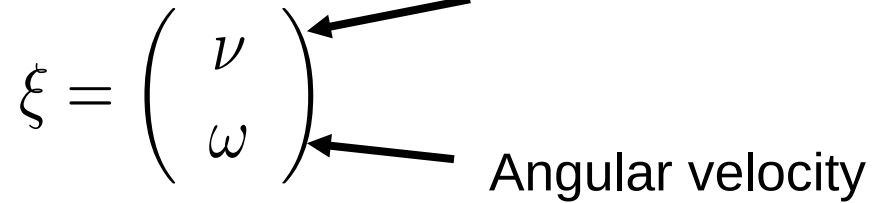
End effector twist:

- Twist is a concatenation of linear velocity and angular velocity: →
- As we will show in a minute, linear and angular velocity have different units

$$\xi = \begin{pmatrix} \nu \\ \omega \end{pmatrix}$$

Linear velocity

Angular velocity



What is Twist?

End effector twist:

- Twist is a concatenation of linear velocity and angular velocity: →
- As we will show in a minute, linear and angular velocity have different units

$$\xi = \begin{pmatrix} \nu \\ \omega \end{pmatrix}$$

Linear velocity

Angular velocity

What is angular velocity?

Angular velocity is a vector that:

- points in the direction of the axis of rotation
- has magnitude equal to the velocity of rotation

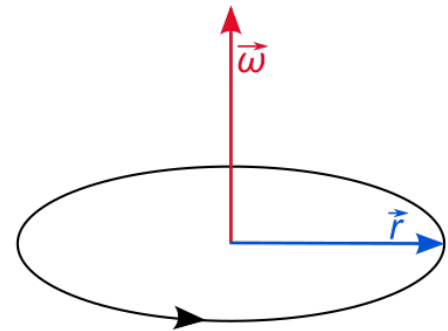
What is Angular Velocity?

Angular velocity is a vector that:

- points in the direction of the axis of rotation
- has magnitude equal to the velocity of rotation

Symbol for angular velocity: ω

Relation between angular velocity and linear velocity: $v = \omega \times r$



We will often write it this way: $\dot{q} = \omega \times q$

Angular Velocity Derivation

$${}^b q = {}^b R_a {}^a q$$

$${}^b \dot{q} = {}^b \dot{R}_a {}^a q \quad \leftarrow \text{Just differentiate all elements of the rotation matrix w.r.t. time.}$$

$${}^b \dot{q} = {}^b \dot{R}_a {}^b R_a^T {}^b q$$

$$S({}^b \omega) = {}^b \dot{R}_a {}^b R_a^T \quad \leftarrow \text{This is the matrix representation of angular velocity}$$

$${}^b \dot{q} = S({}^b \omega) {}^b q \quad \leftarrow \text{This FO differential equation encodes how the particle rotates}$$

Twist: Time out for skew symmetry!

$$S = -S^T \quad \leftarrow \text{Def'n of skew symmetry}$$

$$S = \begin{bmatrix} 0 & a & b \\ -a & 0 & c \\ -b & -c & 0 \end{bmatrix} \quad \leftarrow \text{Skew symmetric matrices always look like this}$$

If you interpret the skew symmetric matrix like this:

$$S(x) = \begin{bmatrix} 0 & -x_z & x_y \\ x_z & 0 & -x_x \\ -x_y & x_x & 0 \end{bmatrix}$$

Then this is another way of writing the cross product:

$$S(x)p = x \times p$$

Angular Velocity Derivation

Skew symmetry of $S({}^b\omega)$:

$$I = {}^bR_a {}^bR_a^T$$

$$0 = {}^b\dot{R}_a {}^bR_a^T + {}^bR_a {}^b\dot{R}_a^T$$

$${}^b\dot{R}_a {}^bR_a^T = -{}^bR_a {}^b\dot{R}_a^T$$

$$S({}^b\omega) = -S({}^b\omega)^T$$

$${}^b\dot{q} = S({}^b\omega) {}^bq$$

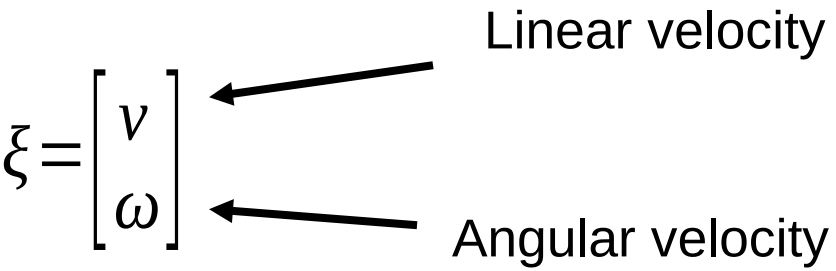
$${}^b\dot{q} = {}^b\omega \times {}^bq$$



You probably already know this formula

Twist

Twist concatenates linear and angular velocity:

$$\xi = \begin{bmatrix} v \\ \omega \end{bmatrix}$$


Linear velocity

Angular velocity

Jacobian

Breakdown of the Jacobian: $v = J_v \dot{q}$

$$\omega = J_\omega \dot{q}$$

$$\xi = \begin{bmatrix} J_v \\ J_\omega \end{bmatrix} \dot{q}$$

Relation to the derivative: $J_v = \frac{\partial x}{\partial q}$ but $J_\omega \neq \frac{\partial r_{\phi\theta\psi}}{\partial q}$

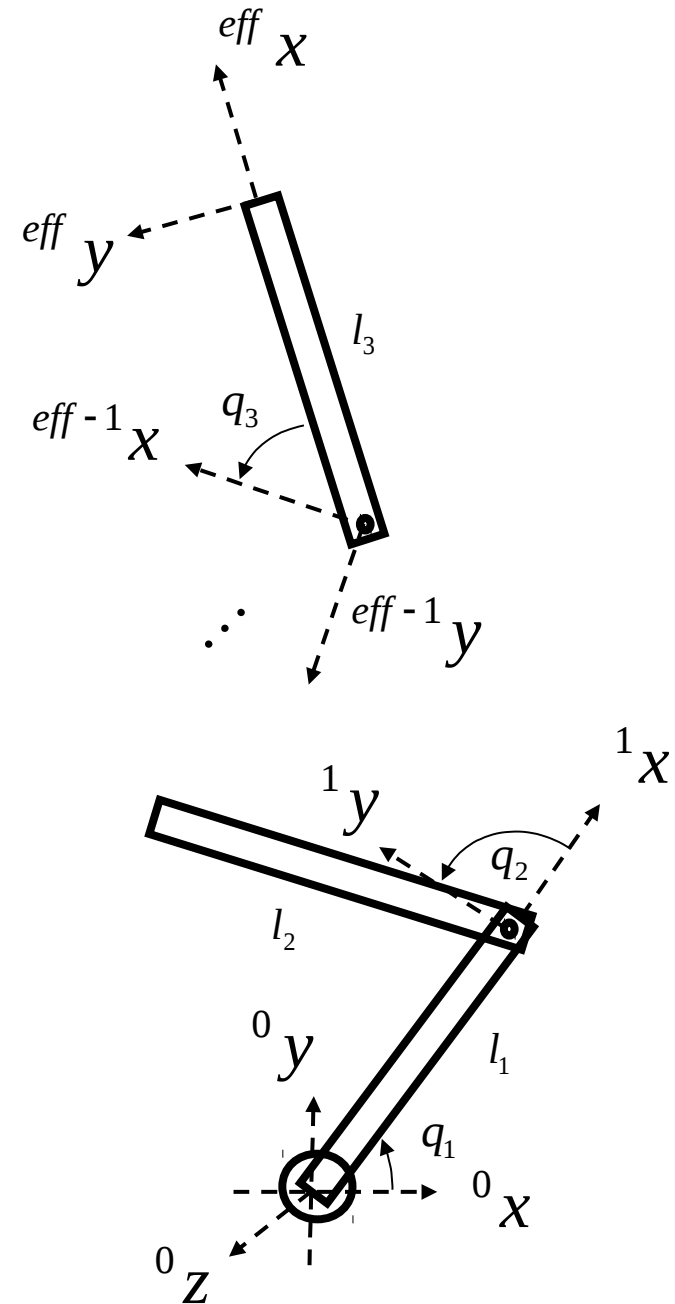


That's not an angular velocity

Calculating the Jacobian

Approach:

- Calculate the Jacobian one column at a time
- Each column describes the motion at the end effector due to the motion of *that joint only*.
- For each joint, i , pretend all the other joints are frozen, and calculate the motion at the end effector caused by i .

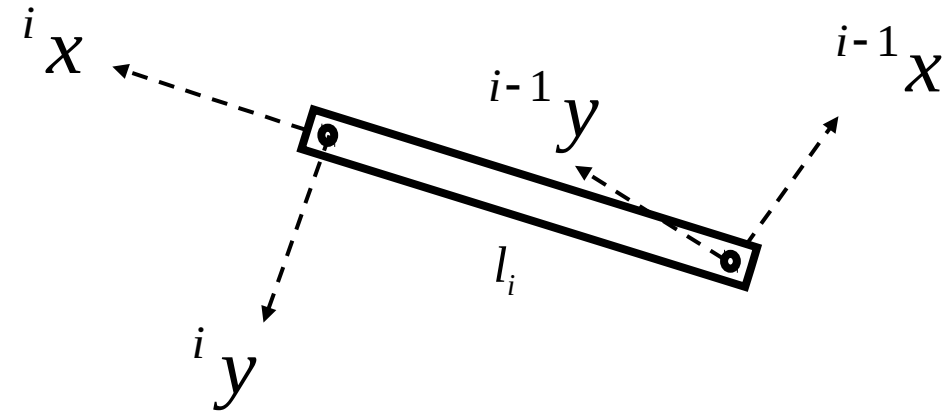


Calculating the Jacobian: Velocity

- The velocity of the end effector caused by motion at the $i-1$ link:

$${}^b \dot{p}_{eff} = \underbrace{{}^b \omega_{i-1} \times}^b p_{i-1,eff} + \underbrace{{}^b \dot{p}_{i-1,i}}$$

Velocity at end effector due to rotation at joint $i-1$



Velocity at end effector due to change in length of link $i-1$

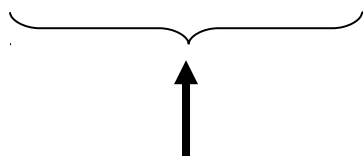
Calculating the Jacobian: Velocity

Rotational DOF

- Rotates about ${}^{i-1}z$

$$J_{v_i} = {}^b z_{i-1} \times {}^b p_{i-1,eff}$$

$$J_{v_i} = {}^b z_{i-1} \times ({}^b p_{eff} - {}^b p_{i-1})$$

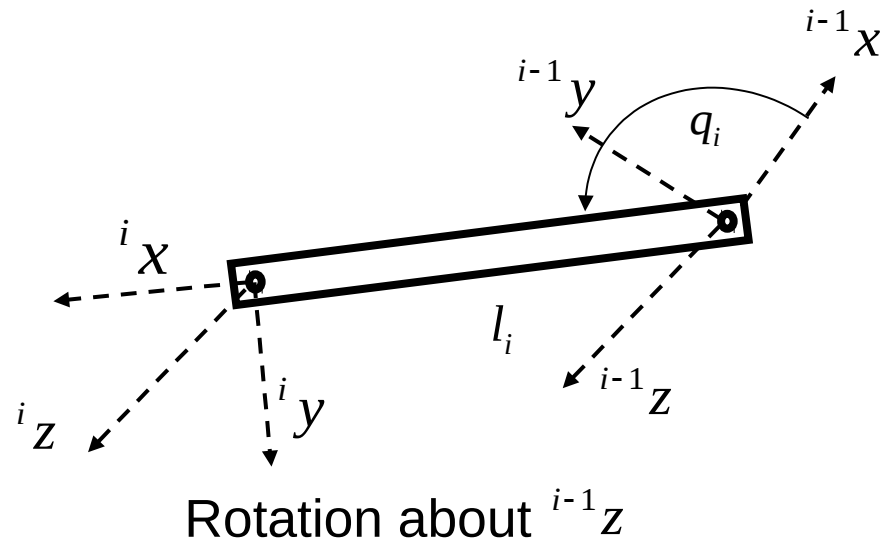


Vector from i-1 to the end effector

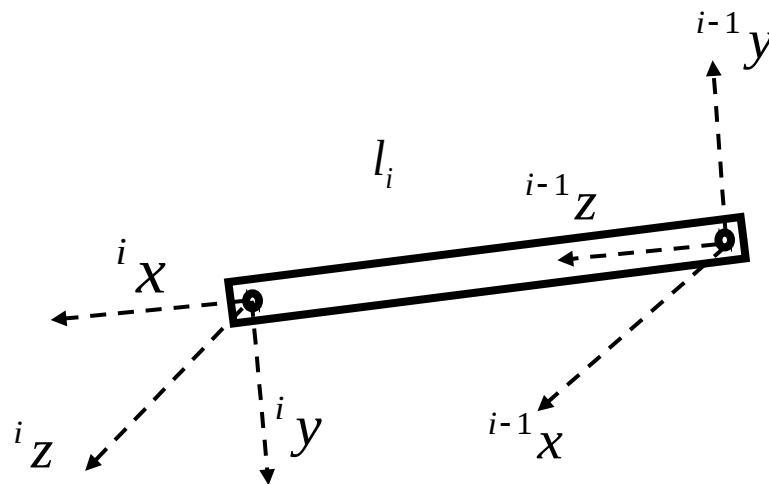
Prismatic DOF

- Translates along ${}^{i-1}z$

$$J_{v_i} = {}^b z_{i-1}$$



Rotation about ${}^{i-1}z$



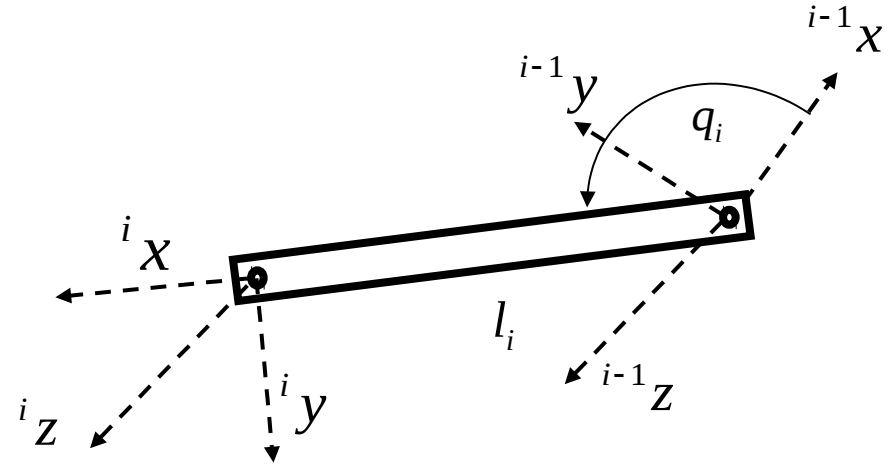
Extension/contraction along ${}^{i-1}z$

Calculating the Jacobian: Velocity

Rotational DOF

- Rotates about ${}^{i-1}z$

$$J_{\omega_i} = {}^b z_{i-1,i}$$

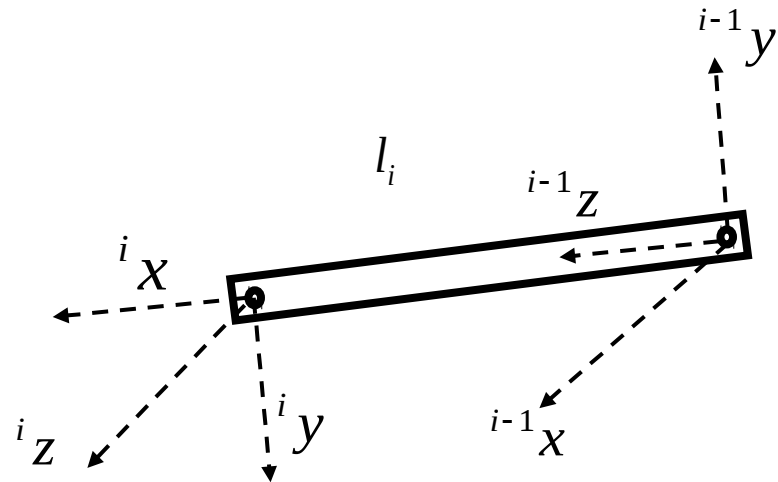


Rotation about ${}^{i-1}z$

Prismatic DOF

- Translates along ${}^{i-1}z$

$$J_{\omega_i} = 0$$



Extension/contraction along ${}^{i-1}z$

Calculating the Jacobian: putting it together

$$J_v = \begin{bmatrix} J_{v_1} & \cdots & J_{v_n} \end{bmatrix}$$

Where

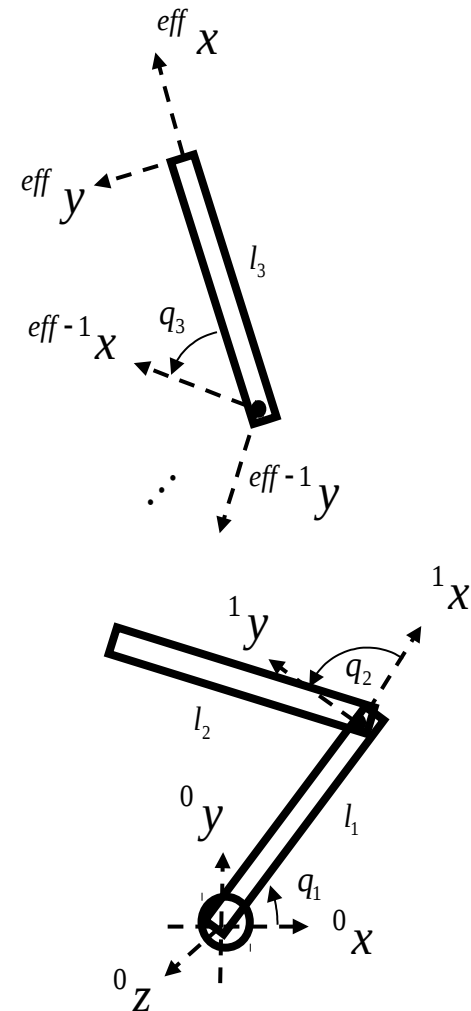
- rotational $J_{v_i} = {}^b Z_{i-1} \times ({}^b p_{eff} - {}^b p_{i-1})$
- prismatic $J_{v_i} = {}^b Z_{i-1}$

$$J_\omega = \begin{bmatrix} J_{\omega_1} & \cdots & J_{\omega_n} \end{bmatrix}$$

Where

- rotational $J_{\omega_i} = {}^b Z_{i-1}$
- prismatic $J_{\omega_i} = 0$

$$J = \begin{bmatrix} J_{v_1} & \cdots & J_{v_n} \\ J_{\omega_1} & \cdots & J_{\omega_n} \end{bmatrix}$$



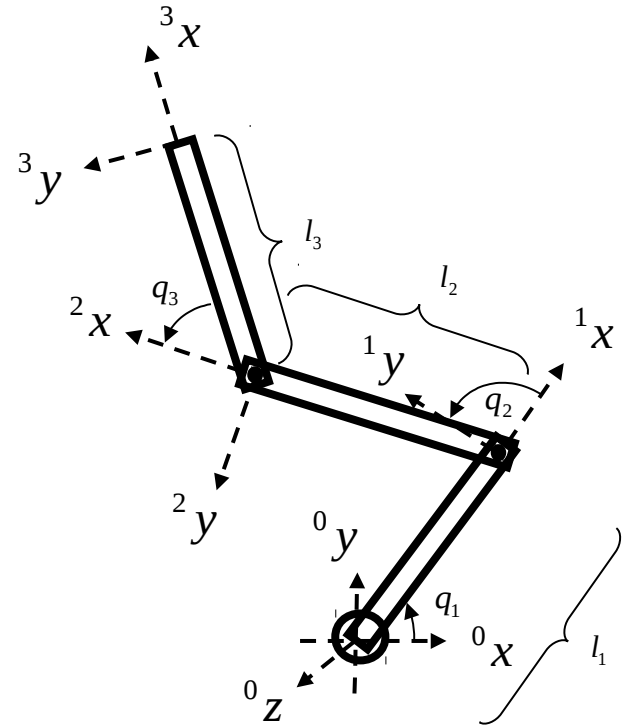
Example 1: calculating the Jacobian

From before:

$${}^0T_1 = \begin{pmatrix} c_{q_1} & -s_{q_1} & 0 & l_1 c_{q_1} \\ s_{q_1} & c_{q_1} & 0 & l_1 s_{q_1} \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{pmatrix} \quad {}^1T_2 = \begin{pmatrix} c_{q_2} & -s_{q_2} & 0 & l_2 c_{q_2} \\ s_{q_2} & c_{q_2} & 0 & l_2 s_{q_2} \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

$${}^2T_3 = \begin{pmatrix} c_{q_3} & -s_{q_3} & 0 & l_3 c_{q_3} \\ s_{q_3} & c_{q_3} & 0 & l_3 s_{q_3} \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

$$J_\omega = \begin{bmatrix} {}^0\hat{z}_0 & {}^0\hat{z}_1 & {}^0\hat{z}_2 \end{bmatrix} = \begin{bmatrix} 0 & 0 & 0 \\ 0 & 0 & 0 \\ 1 & 1 & 1 \end{bmatrix}$$



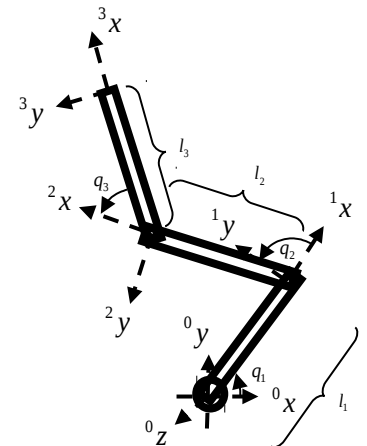
Example 1: calculating the Jacobian

$$J_{v_1} = {}^0 \hat{z}_0 \dot{\iota} ({}^0 o_3 - {}^0 o_0) = \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} \times \left(\begin{bmatrix} l_1 c_1 + l_2 c_{12} + l_3 c_{123} \\ l_1 s_1 + l_2 s_{12} + l_3 s_{123} \\ 0 \end{bmatrix} - \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix} \right) = \begin{bmatrix} -l_1 s_1 - l_2 s_{12} - l_3 s_{123} \\ l_1 c_1 + l_2 c_{12} + l_3 c_{123} \\ 0 \end{bmatrix}$$

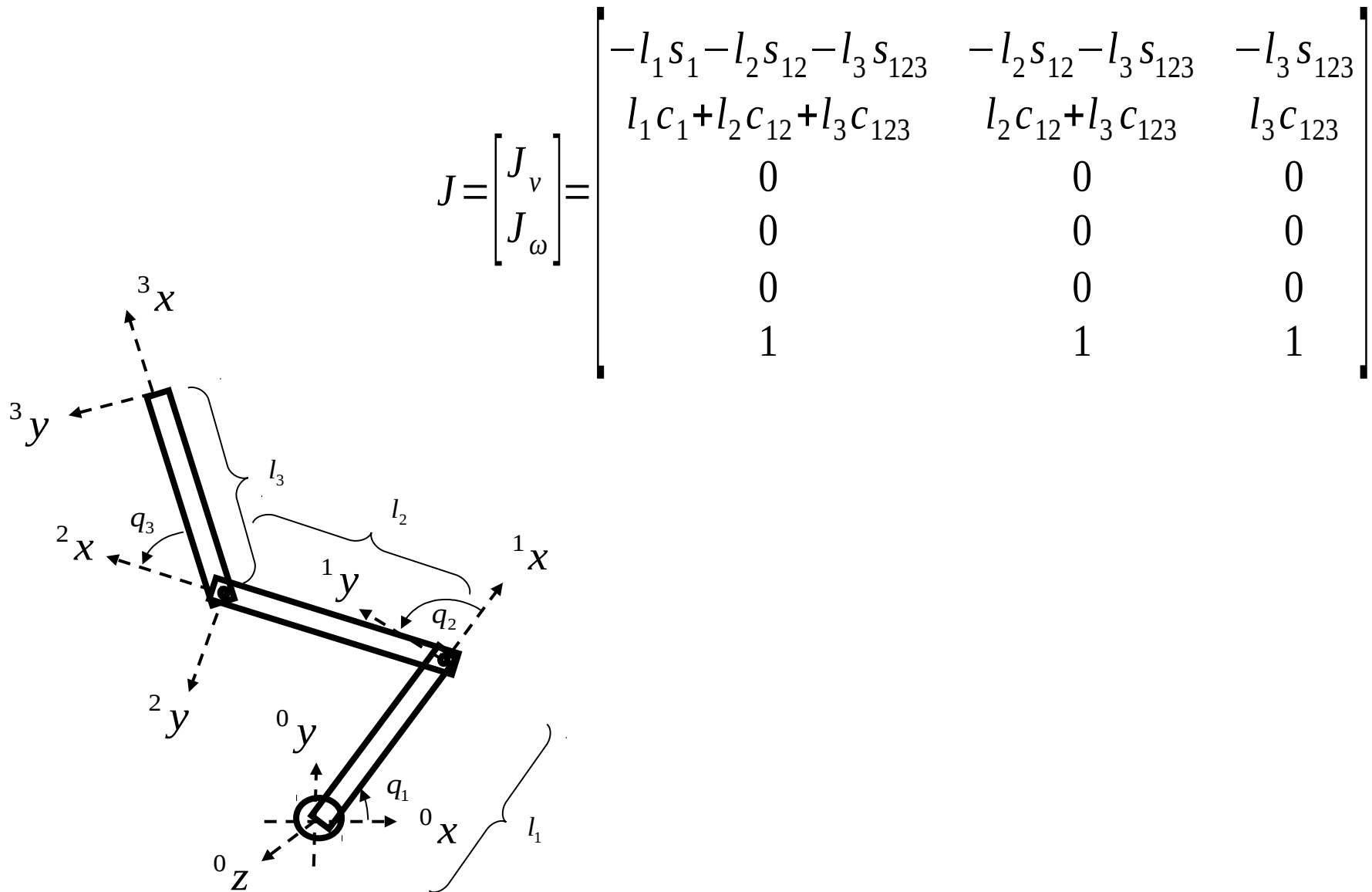
$$J_{v_2} = {}^0 \hat{z}_1 \dot{\iota} ({}^0 o_3 - {}^0 o_1) = \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} \times \left(\begin{bmatrix} l_1 c_1 + l_2 c_{12} + l_3 c_{123} \\ l_1 s_1 + l_2 s_{12} + l_3 s_{123} \\ 0 \end{bmatrix} - \begin{bmatrix} l_1 c_1 \\ l_1 s_1 \\ 0 \end{bmatrix} \right) = \begin{bmatrix} -l_2 s_{12} - l_3 s_{123} \\ l_2 c_{12} + l_3 c_{123} \\ 0 \end{bmatrix}$$

$$J_{v_3} = {}^0 \hat{z}_2 \dot{\iota} ({}^0 o_3 - {}^0 o_2) = \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} \times \left(\begin{bmatrix} l_1 c_1 + l_2 c_{12} + l_3 c_{123} \\ l_1 s_1 + l_2 s_{12} + l_3 s_{123} \\ 0 \end{bmatrix} - \begin{bmatrix} l_1 c_1 + l_2 c_{12} \\ l_1 s_1 + l_2 s_{12} \\ 0 \end{bmatrix} \right) = \begin{bmatrix} -l_3 s_{123} \\ l_3 c_{123} \\ 0 \end{bmatrix}$$

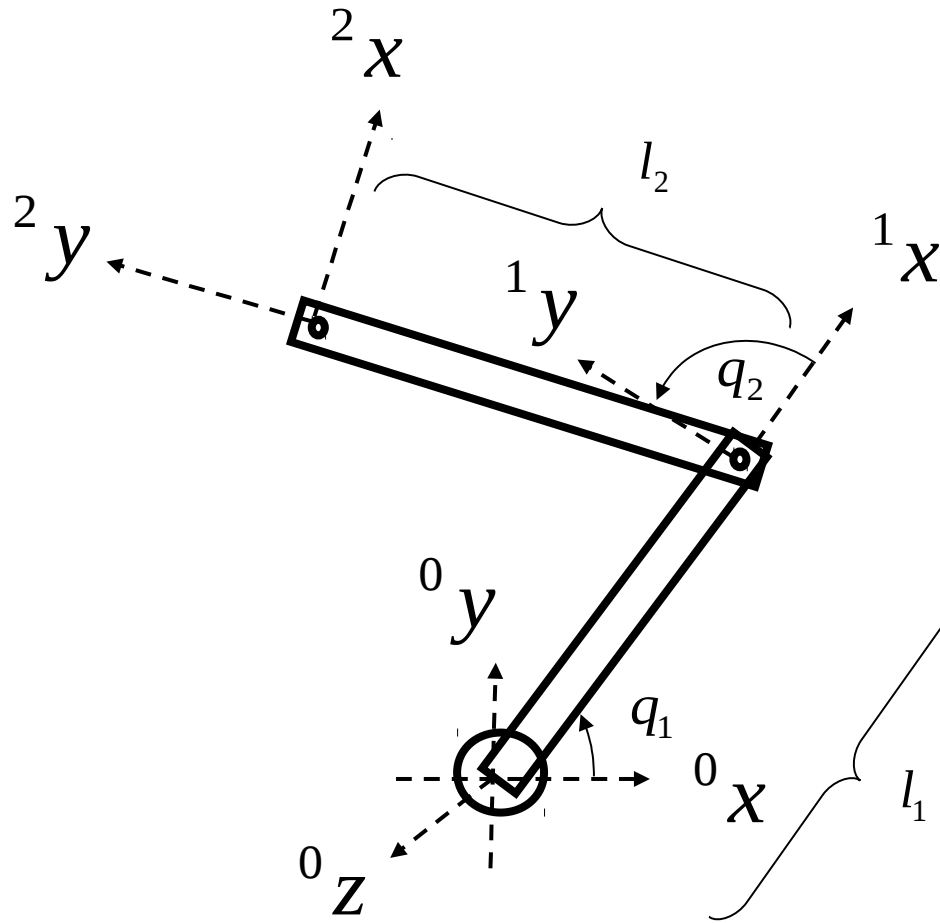
$$J_v = \begin{bmatrix} -l_1 s_1 - l_2 s_{12} - l_3 s_{123} & -l_2 s_{12} - l_3 s_{123} & -l_3 s_{123} \\ l_1 c_1 + l_2 c_{12} + l_3 c_{123} & l_2 c_{12} + l_3 c_{123} & l_3 c_{123} \\ 0 & 0 & 0 \end{bmatrix}$$



Example 1: calculating the Jacobian



Think-pair-share



Calculate the end effector Jacobian
with respect to the base frame

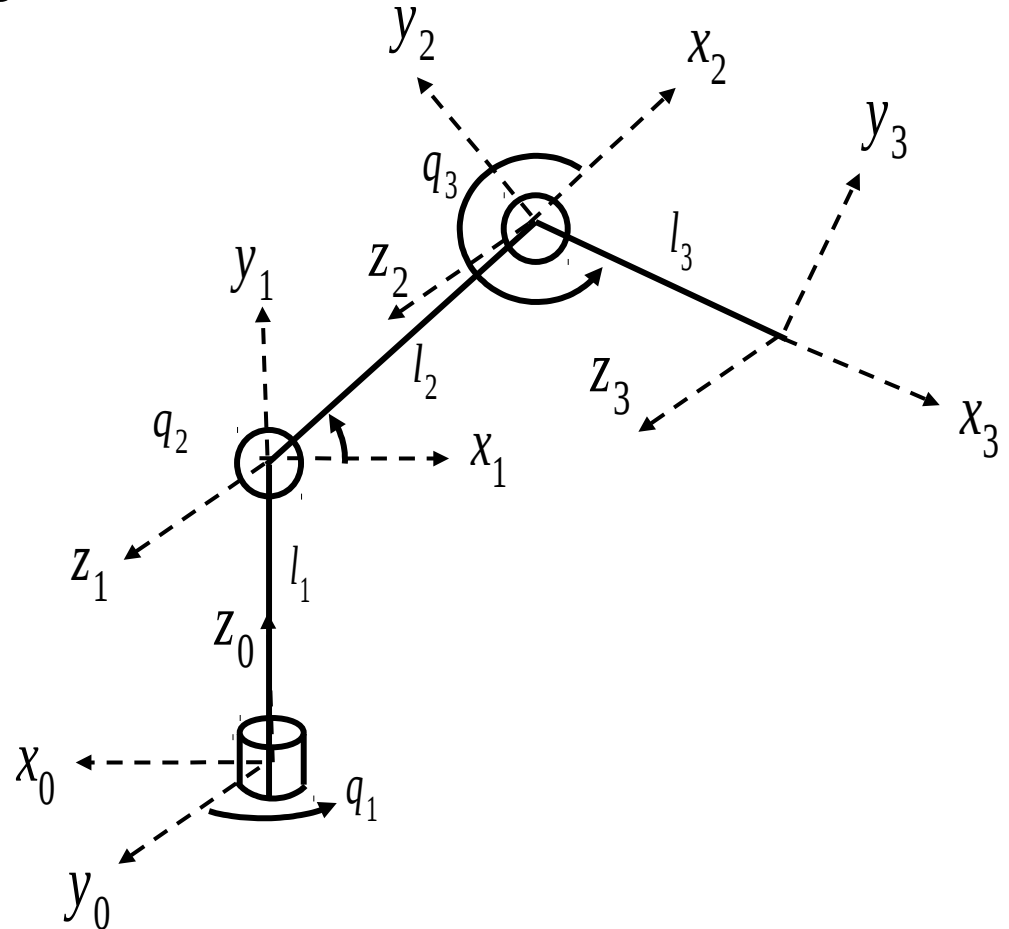
Example 2: calculating the Jacobian

The kinematics of this arm are described by the following:

$${}^0T_1 = \begin{pmatrix} -c_1 & 0 & -s_1 & 0 \\ -s_1 & 0 & c_1 & 0 \\ 0 & 1 & 0 & l_1 \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

$${}^1T_2 = \begin{pmatrix} c_2 & -s_2 & 0 & l_2 c_2 \\ s_2 & c_2 & 0 & l_2 s_2 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

$${}^2T_3 = \begin{pmatrix} c_3 & -s_3 & 0 & l_3 c_3 \\ s_3 & c_3 & 0 & l_3 s_3 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{pmatrix}$$



Example 2: calculating the Jacobian

$${}^b p_0 = \begin{pmatrix} 0 \\ 0 \\ 0 \end{pmatrix}$$

$${}^b z_0 = \begin{pmatrix} 0 \\ 0 \\ 1 \end{pmatrix}$$

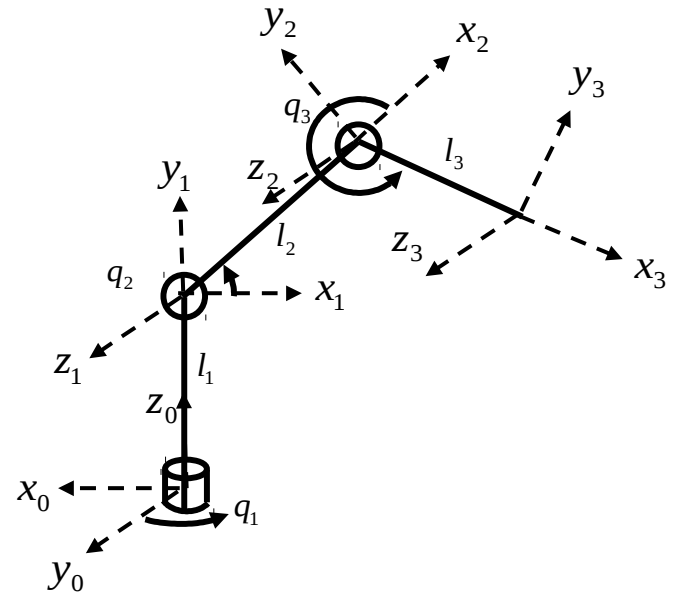
$${}^b p_1 = \begin{pmatrix} 0 \\ 0 \\ l_1 \end{pmatrix}$$

$${}^b z_1 = \begin{pmatrix} -s_1 \\ c_1 \\ 0 \end{pmatrix}$$

$${}^b p_2 = \begin{pmatrix} -l_2 c_1 c_2 \\ -l_2 s_1 c_2 \\ l_2 s_2 + l_1 \end{pmatrix}$$

$${}^b z_2 = \begin{pmatrix} -s_1 \\ c_1 \\ 0 \end{pmatrix}$$

$${}^b p_3 = \begin{pmatrix} -c_1(l_2 c_2 + l_3 c_{23}) \\ -s_1(l_2 c_2 + l_3 c_{23}) \\ l_2 s_2 + l_3 s_{23} + l_1 \end{pmatrix}$$



$$J_{v_1} = {}^b z_0 \times ({}^b p_3 - {}^b p_0)$$

$$J_{v_2} = {}^b z_1 \times ({}^b p_3 - {}^b p_1)$$

$$J_{v_3} = {}^b z_2 \times ({}^b p_3 - {}^b p_2)$$

Example 2: calculating the Jacobian

$$J_{v_1} = \begin{pmatrix} 0 \\ 0 \\ 1 \end{pmatrix} \times \begin{pmatrix} -c_1(l_2 c_2 + l_3 c_{23}) \\ -s_1(l_2 c_2 + l_3 c_{23}) \\ l_2 s_2 + l_3 s_{23} + l_1 \end{pmatrix} = \begin{pmatrix} s_1(l_2 c_2 + l_3 c_{23}) \\ -c_1(l_2 c_2 + l_3 c_{23}) \\ 0 \end{pmatrix}$$

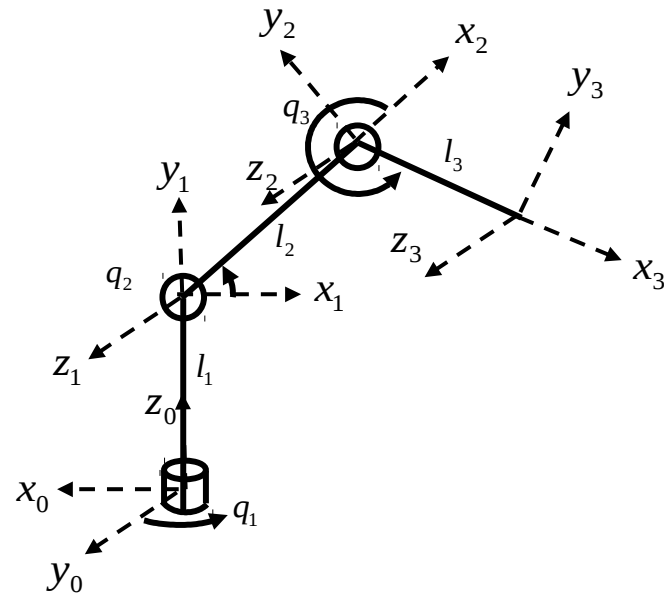
$$J_{\omega_1} = \begin{pmatrix} 0 \\ 0 \\ 1 \end{pmatrix}$$

$$J_{v_2} = \begin{pmatrix} -s_1 \\ c_1 \\ 0 \end{pmatrix} \dot{q}_2 \begin{pmatrix} -c_1(l_2 c_2 + l_3 c_{23}) \\ -s_1(l_2 c_2 + l_3 c_{23}) \\ l_2 s_2 + l_3 s_{23} \end{pmatrix} = \begin{pmatrix} c_1(l_2 c_2 + l_3 c_{23}) \\ s_1(l_2 c_2 + l_3 c_{23}) \\ l_2 c_2 + l_3 c_{23} \end{pmatrix}$$

$$J_{\omega_2} = \begin{pmatrix} -s_1 \\ c_1 \\ 0 \end{pmatrix}$$

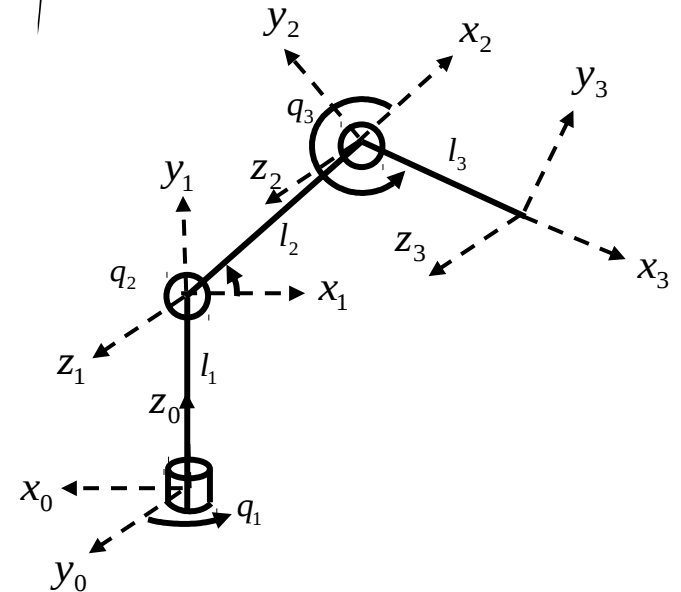
$$J_{v_3} = \begin{pmatrix} -s_1 \\ c_1 \\ 0 \end{pmatrix} \dot{q}_3 \begin{pmatrix} -c_1 l_3 c_{23} \\ -s_1 l_3 c_{23} \\ l_3 s_{23} \end{pmatrix} = \begin{pmatrix} l_3 c_1 s_{23} \\ l_3 s_1 s_{23} \\ l_3 c_{23} \end{pmatrix}$$

$$J_{\omega_3} = \begin{pmatrix} -s_1 \\ c_1 \\ 0 \end{pmatrix}$$



Example 2: calculating the Jacobian

$$J = \begin{pmatrix} s_1(l_2 c_2 + l_3 c_{23}) & c_1(l_2 c_2 + l_3 c_{23}) & l_3 c_1 s_{23} \\ -c_1(l_2 c_2 + l_3 c_{23}) & s_1(l_2 c_2 + l_3 c_{23}) & l_3 c_1 s_{23} \\ 0 & l_2 c_2 + l_3 c_{23} & l_3 c_{23} \\ 0 & -s_1 & -s_1 \\ 0 & c_1 & c_1 \\ 1 & 0 & 0 \end{pmatrix}$$



Expressing the Jacobian in Different Reference Frames

In the preceding, the Jacobian has been expressed in the base frame

- It can be expressed in other reference frames using rotation matrices

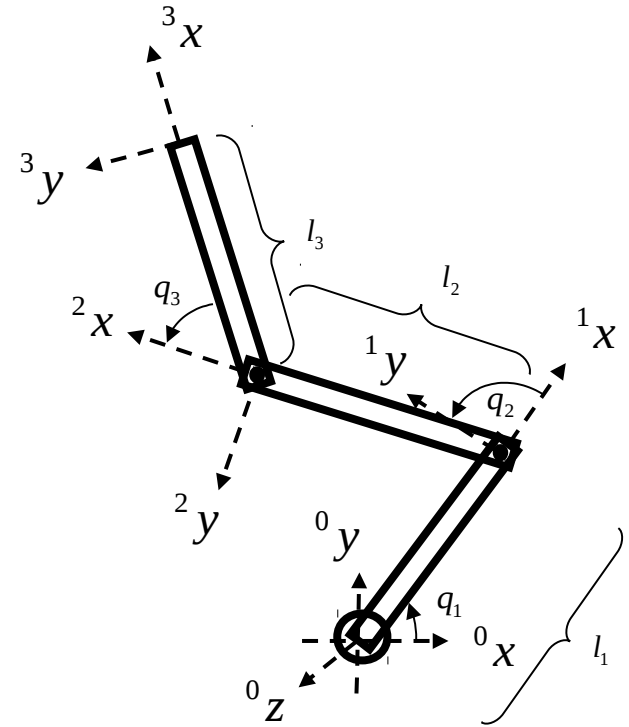
Velocity is transformed from one reference frame to another using:

$${}^k p = {}^k R_b {}^b p$$

$${}^k \dot{p} = {}^k R_b {}^b \dot{p}$$

Therefore, the velocity Jacobian can be transformed using:

$${}^k J_v = {}^k R_b {}^b J_v$$



Expressing the Jacobian in Different Reference Frames

First, let's express angular velocity in a different reference frame:

$${}^b \dot{p} = S({}^b \omega) {}^b p \quad \longleftarrow \text{Def'n of angular velocity}$$

$${}^k R_b {}^b \dot{p} = {}^k R_b S({}^b \omega) {}^b p$$

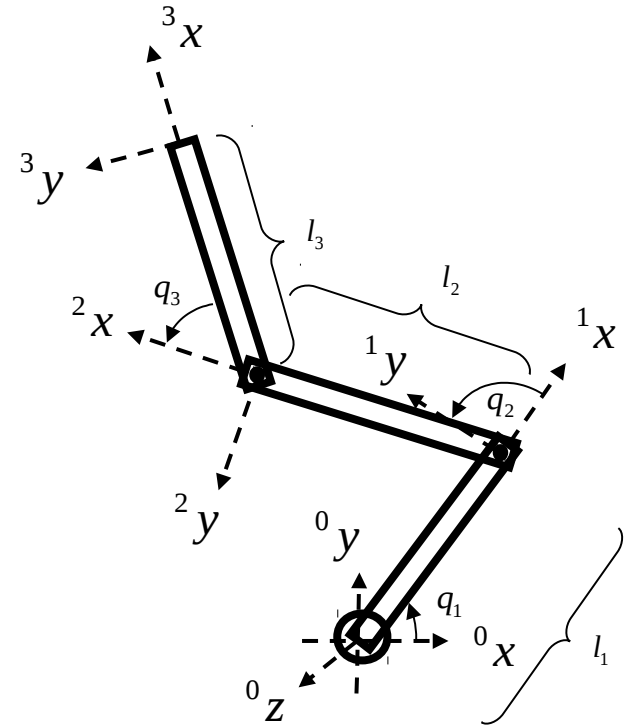
$${}^k \dot{p} = {}^k R_b S({}^b \omega) {}^k R_b^T {}^k p$$

$${}^k \dot{p} = S({}^k R_b {}^b \omega) {}^k p$$

$${}^k \omega = {}^k R_b {}^b \omega \quad \longleftarrow \text{Angular velocity can also be rotated by a rotation matrix}$$

Therefore, the angular velocity Jacobian can be transformed using:

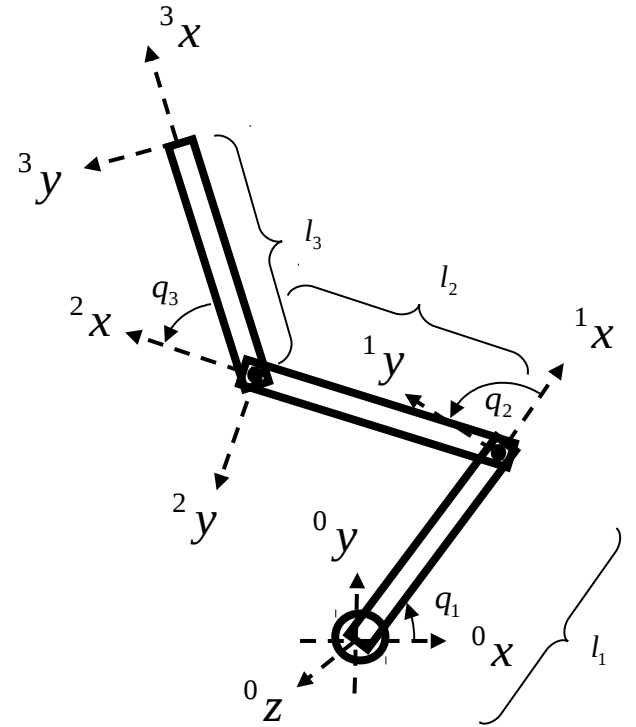
$${}^k J_\omega = {}^k R_b {}^b J_\omega$$



Expressing the Jacobian in Different Reference Frames

Therefore, the full Jacobian is rotated:

$${}^k J = \begin{pmatrix} {}^k R_b & 0 \\ 0 & {}^k R_b \end{pmatrix} {}^b J$$

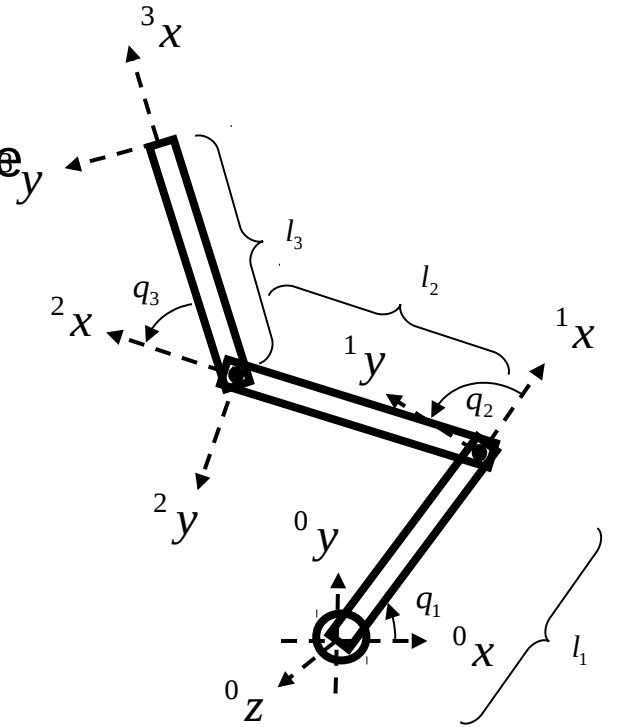


Different Jacobian Reference Frames: Example

Express the Jacobian for the three-link arm in the reference frame of the end effector:

$${}^0 R_3 = \begin{pmatrix} c_{123} & -s_{123} & 0 \\ s_{123} & c_{123} & 0 \\ 0 & 0 & 1 \end{pmatrix}$$

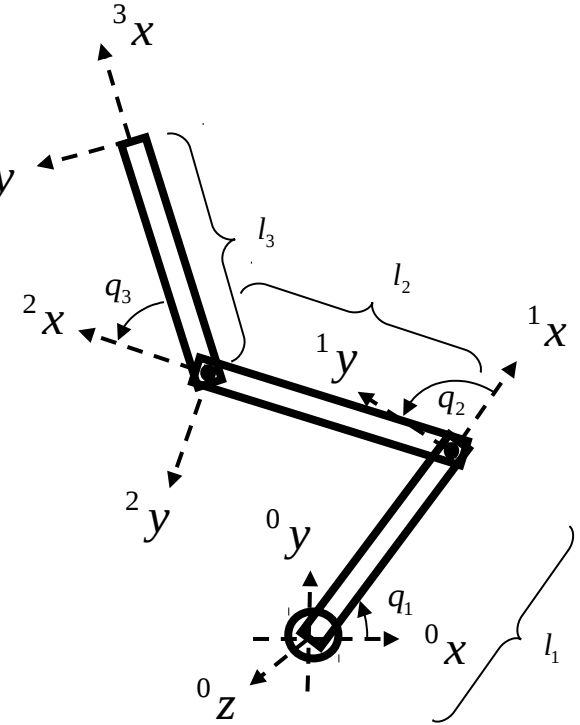
$$J = \begin{bmatrix} -l_1 s_1 - l_2 s_{12} - l_3 s_{123} & -l_2 s_{12} - l_3 s_{123} & -l_3 s_{123} \\ l_1 c_1 + l_2 c_{12} + l_3 c_{123} & l_2 c_{12} + l_3 c_{123} & l_3 c_{123} \\ 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \\ 1 & 1 & 1 \end{bmatrix}$$



Different Jacobian Reference Frames: Example

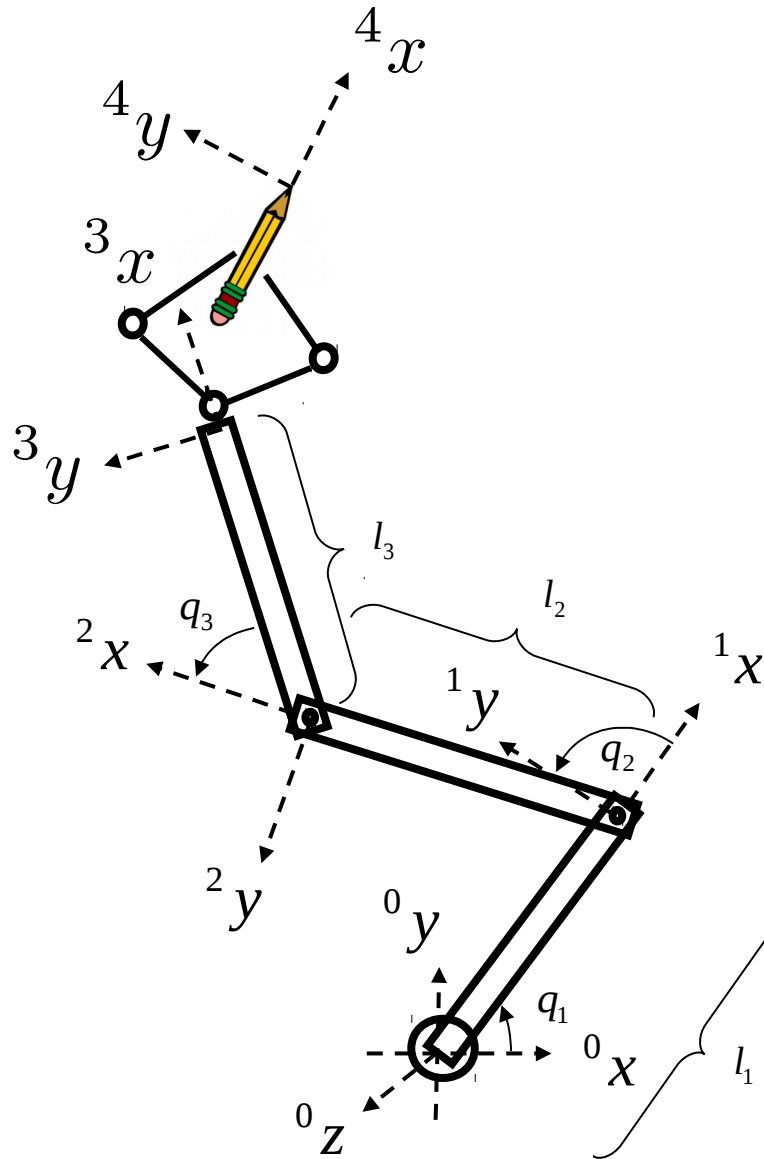
Express the Jacobian for the three-link arm in the reference frame of the end effector:

$${}^0 R_3 = \begin{pmatrix} c_{123} & -s_{123} & 0 \\ s_{123} & c_{123} & 0 \\ 0 & 0 & 1 \end{pmatrix}$$



$${}^3 J = \begin{pmatrix} c_{123} & s_{123} & 0 & 0 & 0 & 0 & -l_1 s_1 - l_2 s_{12} - l_3 s_{123} & -l_2 s_{12} - l_3 s_{123} & -l_3 s_{123} \\ -s_{123} & c_{123} & 0 & 0 & 0 & 0 & l_1 c_1 + l_2 c_{12} + l_3 c_{123} & l_2 c_{12} + l_3 c_{123} & l_3 c_{123} \\ 0 & 0 & 1 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & c_{123} & s_{123} & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & -s_{123} & c_{123} & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 & 1 & 1 & 1 \end{pmatrix}$$

Think-pair-share



Given 0J (in base frame)

Given: 3R_0 and 4R_3

Calculate: 4J