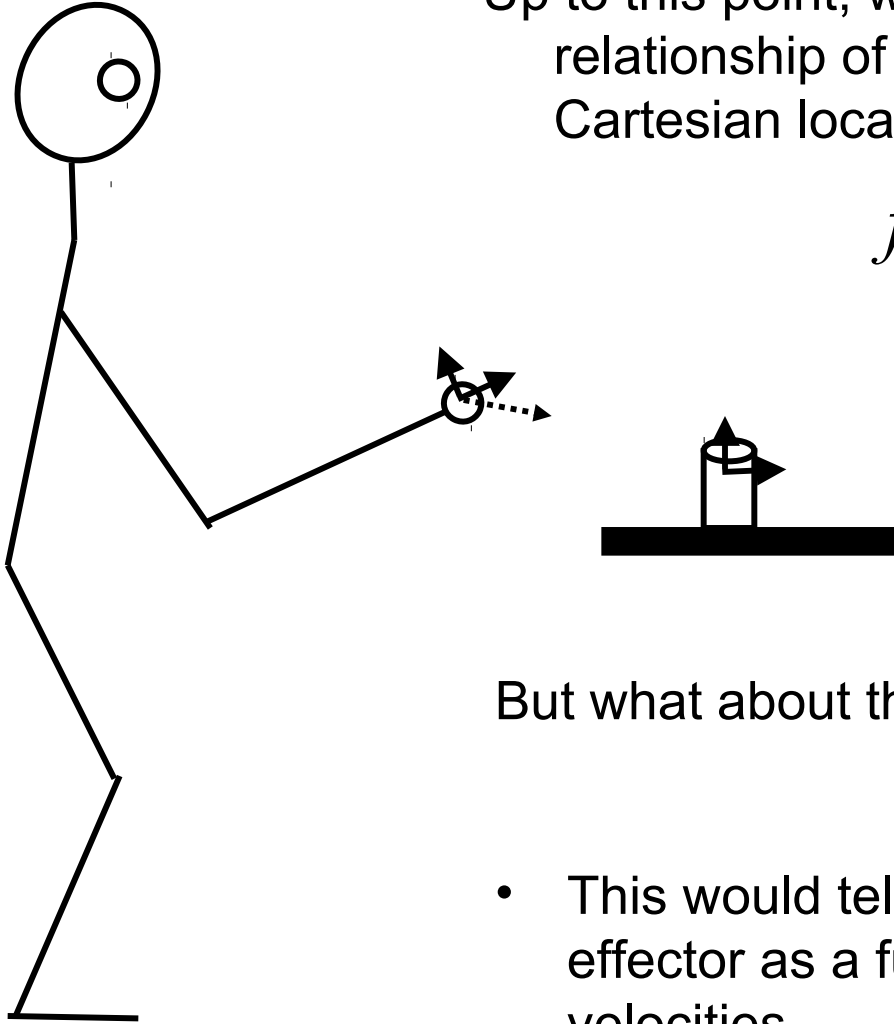


Differential Kinematics

Up to this point, we have only considered the relationship of the joint angles to the Cartesian location of the end effector:

$$f(q) = x$$



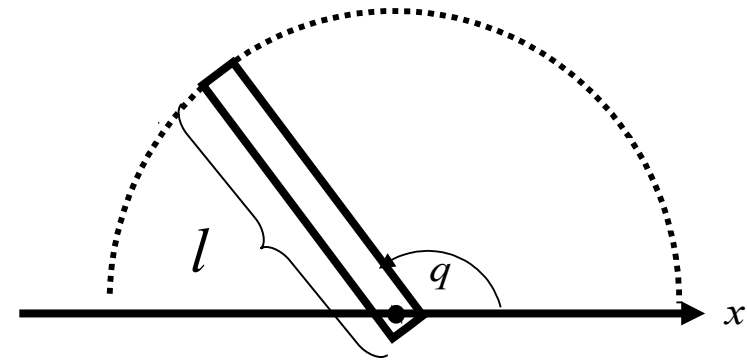
But what about the first derivative? $\frac{\partial f(q)}{\partial q}$

- This would tell us the velocity of the end effector as a function of joint angle velocities.

Motivating Example

Consider a one-link arm

- As the arm rotates, the end effector sweeps out an arc
- Let's assume that we are only interested in the x coordinate...



Forward kinematics: $x = l \cos(q)$

Differential kinematics: $\frac{dx}{dq} = -l \sin(q)$

$$\delta x = -l \sin(q) \delta q$$

$$\delta q = -\frac{1}{l \sin(q)} \delta x$$

Motivating Example

Suppose you want to move the end effector above a specified point, x_g

Answer #1: $q_g = \cos^{-1}\left(\frac{x_g}{l}\right)$

Answer #2: 1. $i = 0, q_0 = \text{arbitrary}$

2. $x_i = l \cos(q_i)$

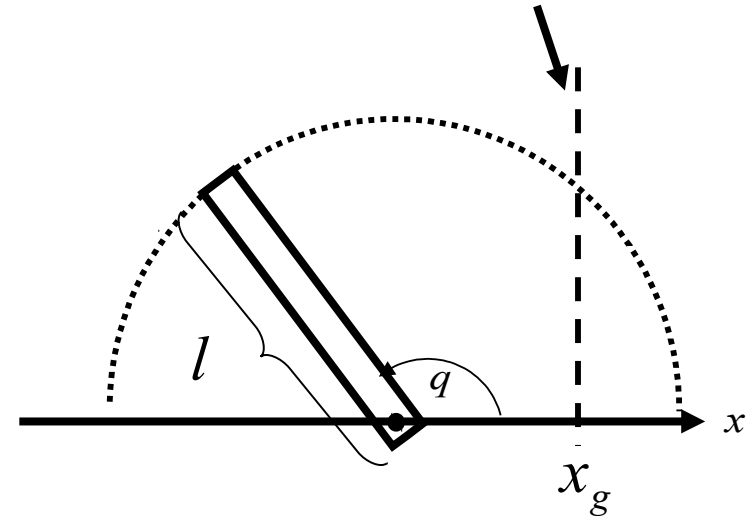
3. $\delta x = \alpha(x_g - x_i)$

4. $\delta q = \frac{1}{-l \sin(q_i)} \delta x$

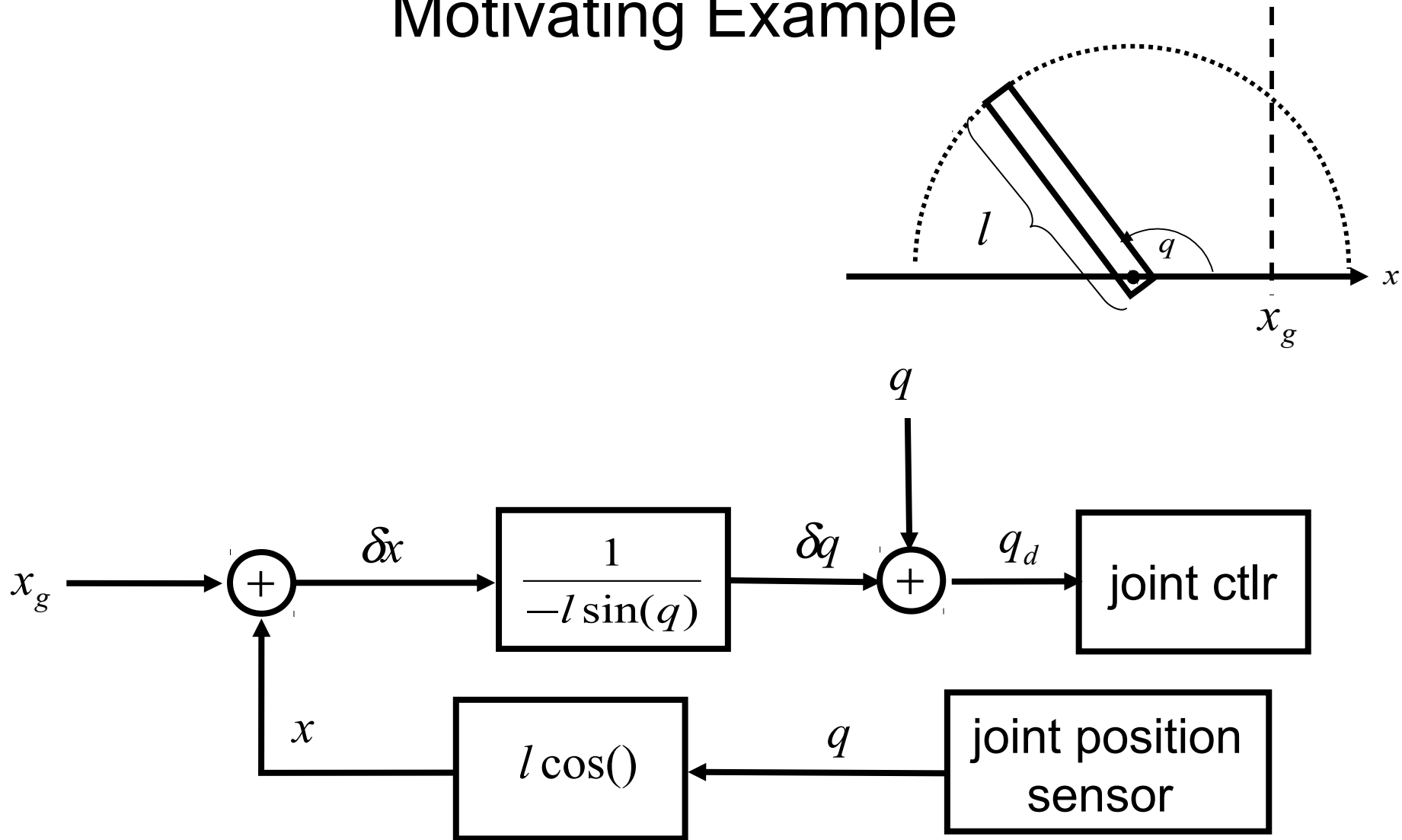
5. $q_{i+1} = q_i + \delta q$

6. $i++$ goto 2.

Goal: move the end effector onto this line



Motivating Example



This controller moves the link asymptotically toward the goal position.

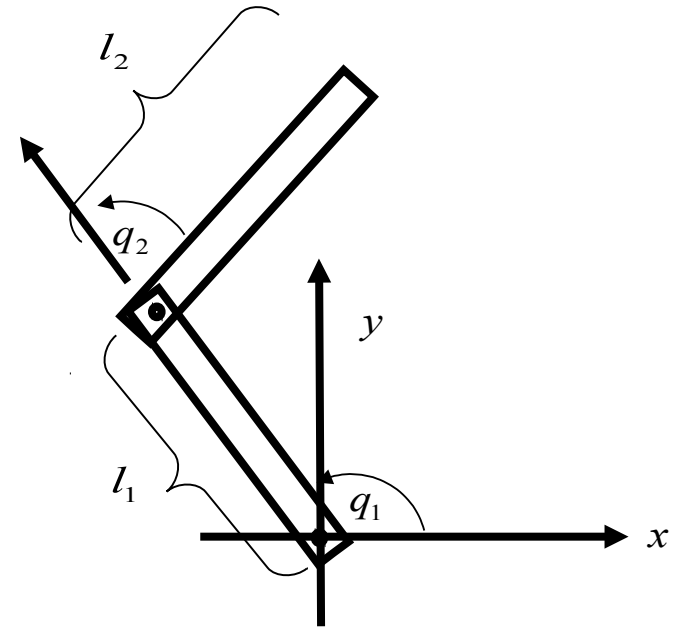
Intro to the Jacobian

$$\vec{x} = \begin{bmatrix} l_1 \cos(q_1) + l_2 \cos(q_1 + q_2) \\ l_1 \sin(q_1) + l_2 \sin(q_1 + q_2) \end{bmatrix} \quad \leftarrow \text{Forward kinematics of the two-link manipulator}$$

Velocity Jacobian



$$\frac{d\vec{x}}{dq} = \begin{bmatrix} -l_1 \sin(q_1) - l_2 \sin(q_1 + q_2) & -l_2 \sin(q_1 + q_2) \\ l_1 \cos(q_1) + l_2 \cos(q_1 + q_2) & l_2 \cos(q_1 + q_2) \end{bmatrix}$$
$$= J(q)$$

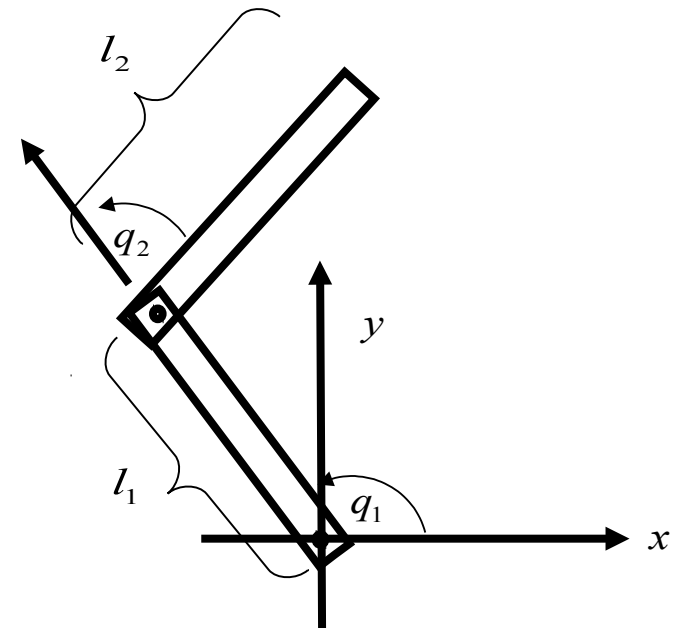
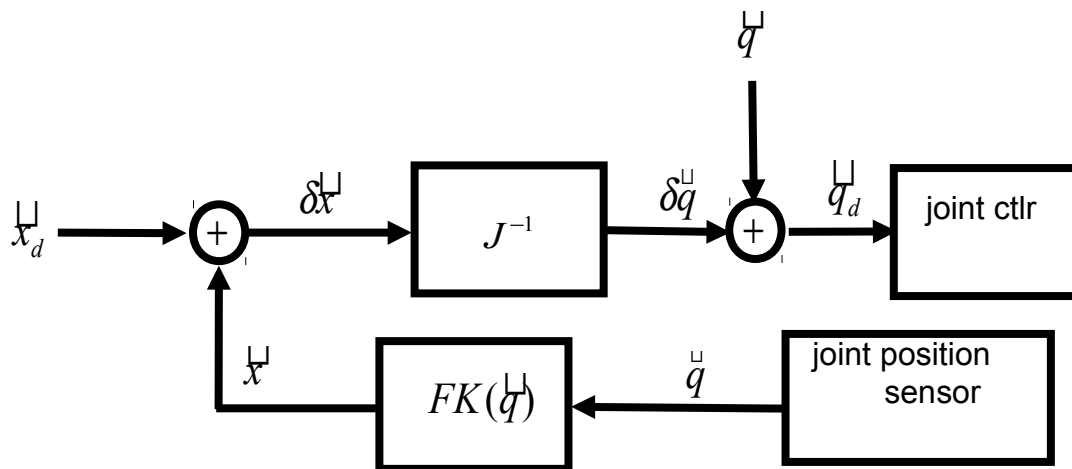


Intro to the Jacobian

$$J(q) = \begin{bmatrix} -l_1 \sin(q_1) - l_2 \sin(q_1 + q_2) & -l_2 \sin(q_1 + q_2) \\ l_1 \cos(q_1) + l_2 \cos(q_1 + q_2) & l_2 \cos(q_1 + q_2) \end{bmatrix}$$

Chain rule: $\delta x = J \delta q$

If the Jacobian is square and full rank, then we can invert it: $\delta q = J^{-1} \delta x$



Jacobian

The Jacobian relates joint velocities with end effector *twist*:

$$\xi = J\dot{q}$$

End effector twist

Jacobian

Joint angle velocities

- First derivative of joint angles:

$$\dot{q} = \begin{bmatrix} \dot{q}_1 \\ \vdots \\ \dot{q}_n \end{bmatrix}$$

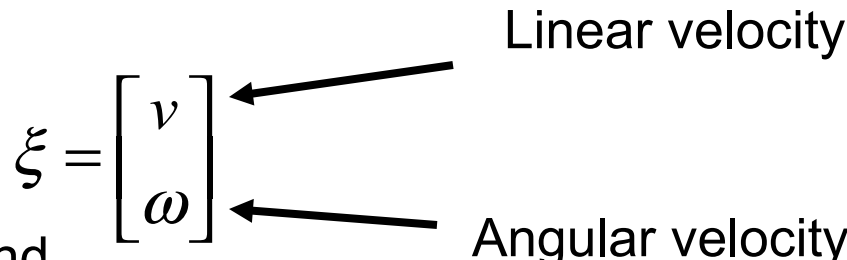
It turns out that you can “easily” compute the Jacobian for arbitrary manipulator structures

- This makes differential kinematics a much easier sub-problem than kinematics in general.

What is Twist?

End effector twist:

- Twist is a concatenation of linear velocity and angular velocity:
- As we will show in a minute, linear and angular velocity have different units
 - Although we will frequently treat this quantity as a 6-vector, it is NOT one...

$$\xi = \begin{bmatrix} v \\ \omega \end{bmatrix}$$


Linear velocity

Angular velocity

Twist: Angular Velocity

$${}^b q = {}^b R_a {}^a q$$

$${}^b \dot{q} = {}^b \dot{R}_a {}^a q \quad \longleftarrow \text{Just differentiate all elements of the rotation matrix w.r.t. time.}$$

$${}^b \dot{q} = {}^b \dot{R}_a {}^b R_a^T {}^b q$$

$$S({}^b \omega) = {}^b \dot{R}_a \underbrace{{}^b R_a^T}_{\text{matrix representation of angular velocity}}$$

$${}^b \dot{q} = S({}^b \omega) {}^b q \quad \longleftarrow \text{This FO differential equation encodes how the particle rotates}$$

FYI: this expression can be solved using an exponential:

$${}^b q(t) = e^{S({}^b \omega)t} {}^b q(0) = \left[I + S({}^b \omega)t + \frac{(S({}^b \omega)t)^2}{2} + \dots \right] q(0)$$

Twist: Angular Velocity

$$\begin{aligned} {}^b q(t) &= e^{S({}^b \omega)t} {}^b q(0) = \left[I + S({}^b \omega)t + \frac{(S({}^b \omega)t)^2}{2} + \dots \right] q(0) \\ &= \left[I + S({}^b \omega)t \sin(\theta) + S({}^b \omega)^2 t^2 (1 - \cos(\theta)) \right] q(0) \end{aligned}$$

Twist: Time out for skew symmetry!

$$S = -S^T \quad \longleftarrow \text{Def'n of skew symmetry}$$

$$S = \begin{bmatrix} 0 & a & b \\ -a & 0 & c \\ -b & -c & 0 \end{bmatrix} \quad \longleftarrow \text{Skew symmetric matrices always look like this}$$

If you interpret the skew symmetric matrix like this:

$$S(x) = \begin{bmatrix} 0 & -x_z & x_y \\ x_z & 0 & -x_x \\ -x_y & x_x & 0 \end{bmatrix}$$

Then this is another way of writing the cross product:

$$S(x)p = x \times p$$

Twist: Angular Velocity

Skew symmetry of $S({}^b\omega)$:

$$I = {}^bR_a {}^bR_a^T$$

$$0 = {}^b\dot{R}_a {}^bR_a^T + {}^bR_a {}^b\dot{R}_a^T$$

$${}^b\dot{R}_a {}^bR_a^T = - {}^bR_a {}^b\dot{R}_a^T$$

$$S({}^b\omega) = -S({}^b\omega)^T$$

$${}^b\dot{q} = S({}^b\omega) {}^bq$$

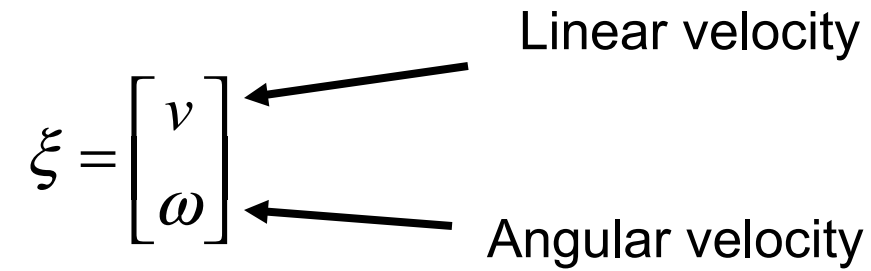
$${}^b\dot{q} = {}^b\omega \times {}^bq$$



You probably already know this formula

Twist

Twist concatenates linear and angular velocity:

$$\xi = \begin{bmatrix} v \\ \omega \end{bmatrix}$$


Linear velocity

Angular velocity

Jacobian

Breakdown of the Jacobian: $v = J_v \dot{q}$

$$\omega = J_\omega \dot{q}$$

$$\xi = \begin{bmatrix} J_v \\ J_\omega \end{bmatrix} \dot{q}$$

Relation to the derivative: $J_v = \frac{\partial x}{\partial q}$ **but** $J_\omega \neq \frac{\partial r_{\phi\theta\psi}}{\partial q}$

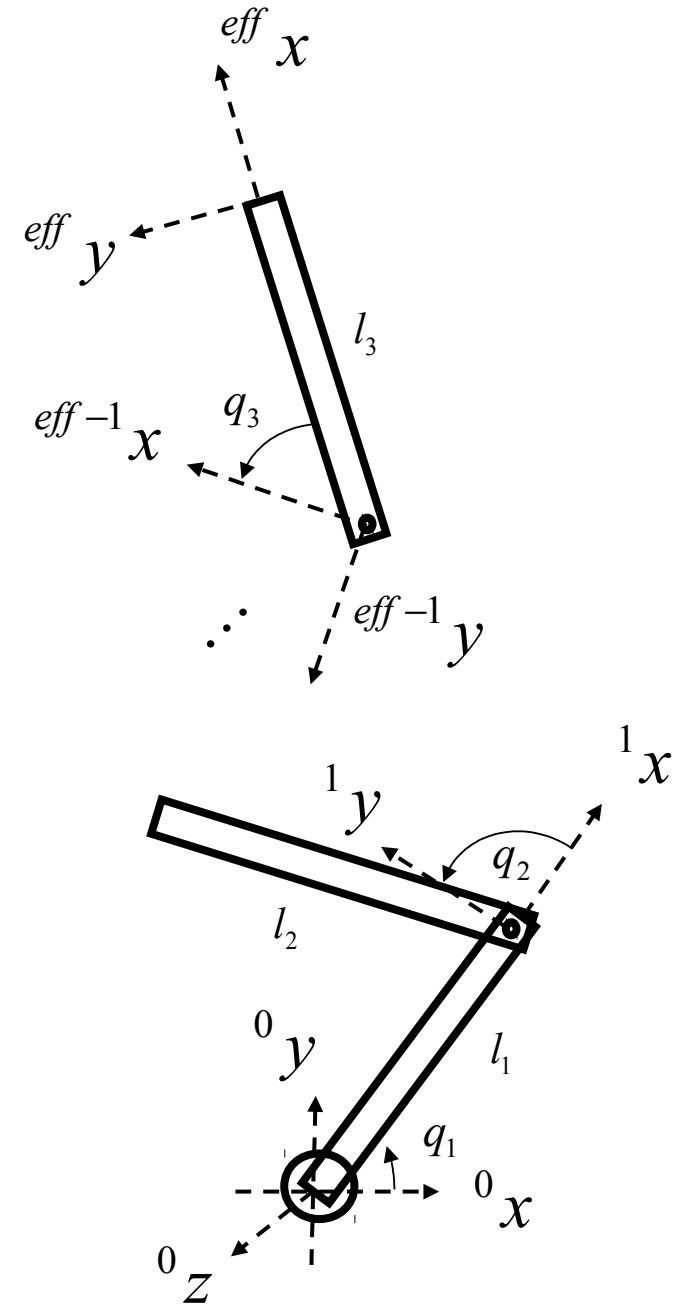


That's not an angular velocity

Calculating the Jacobian

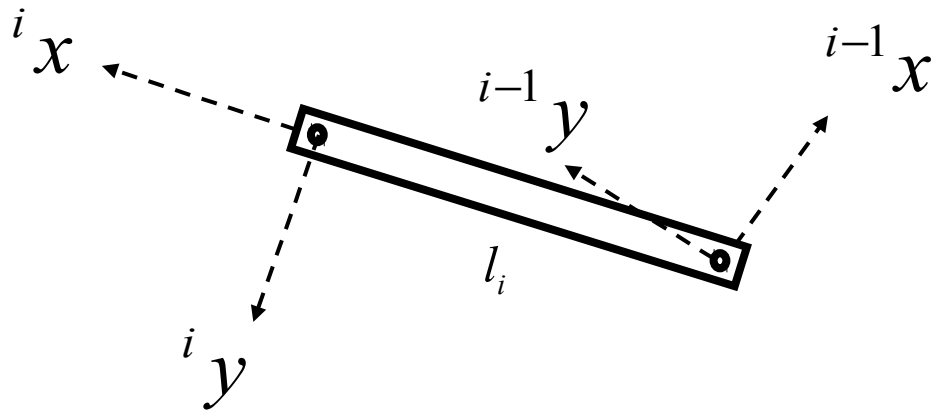
Approach:

- Calculate the Jacobian one column at a time
- Each column describes the motion at the end effector due to the motion of *that joint only*.
- For each joint, i , pretend all the other joints are frozen, and calculate the motion at the end effector caused by i .



Calculating the Jacobian: Velocity

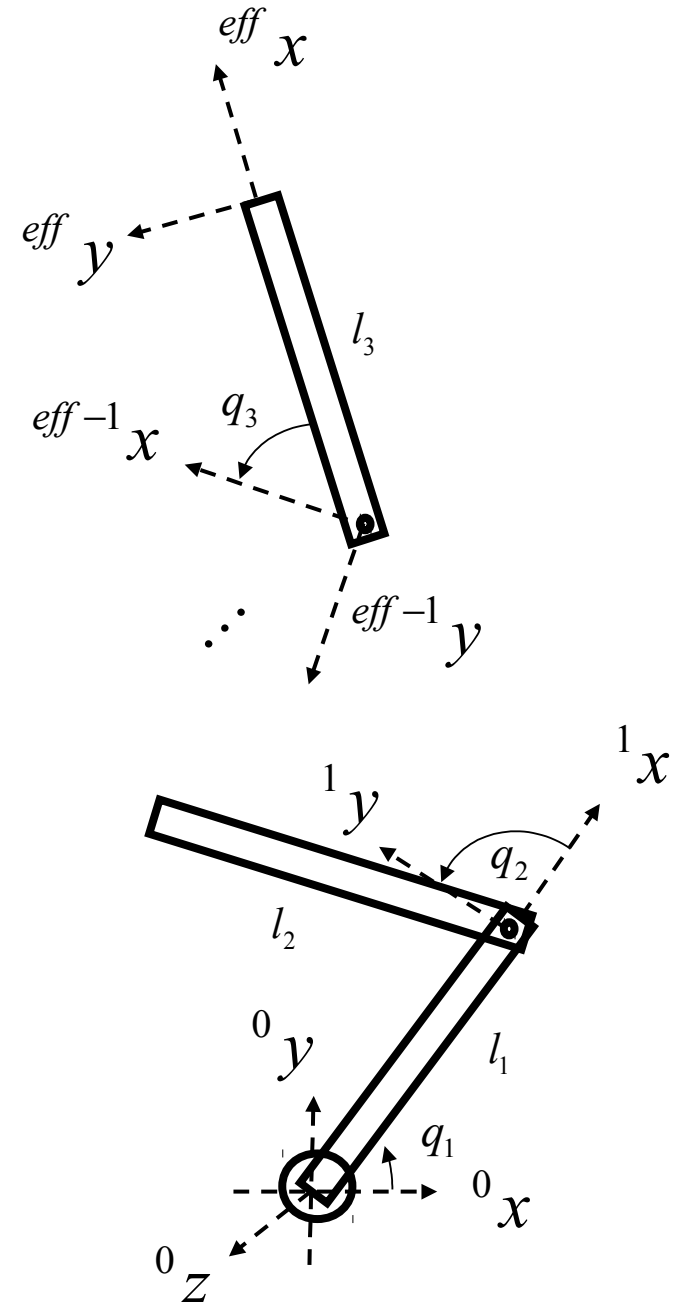
How does the end effector translate as the i^{th} link moves?



$${}^b p_{eff} = {}^b R_{i-1} {}^{i-1} p_{i-1, eff}$$

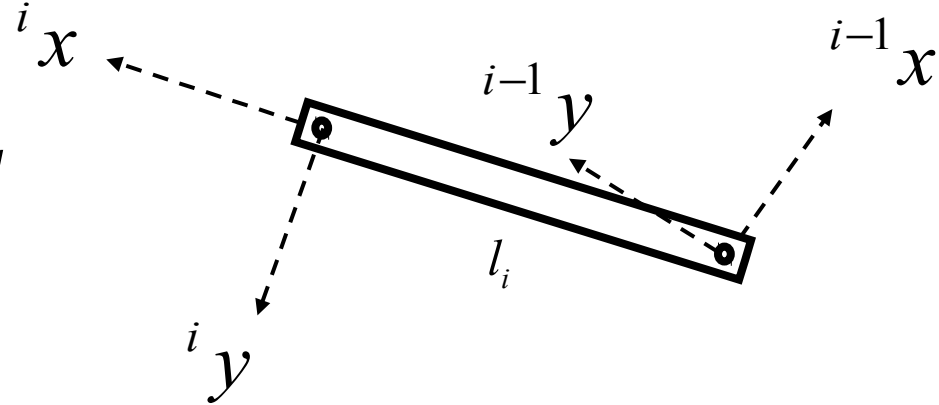
Orientation of the $i-1^{th}$ link

Vector from reference frame $i-1$ to the end effector



Calculating the Jacobian: Velocity

- Calculate the velocity of the end effector caused by motion at the $i-1$ link:



$${}^b p_{eff} = {}^b R_{i-1} {}^{i-1} p_{i-1,eff}$$

$${}^b \dot{p}_{eff} = {}^b \dot{R}_{i-1} {}^{i-1} p_{i-1,eff} + {}^b R_{i-1} {}^{i-1} \dot{p}_{i-1,eff}$$

$${}^b \dot{p}_{eff} = {}^b \dot{R}_{i-1} {}^b R_{i-1}^T {}^b R_{i-1} {}^{i-1} p_{i-1,eff} + {}^b \dot{p}_{i-1,eff}$$

$$S({}^b \omega_{i-1}) = {}^b \dot{R}_{i-1} {}^b R_{i-1}^T$$

$${}^b \dot{p}_{eff} = S({}^b \omega_{i-1}) {}^b p_{i-1,eff} + {}^b \dot{p}_{i-1,eff}$$

$${}^b \dot{p}_{eff} = {}^b \omega_{i-1} \times {}^b p_{i-1,eff} + {}^b \dot{p}_{i-1,i}$$

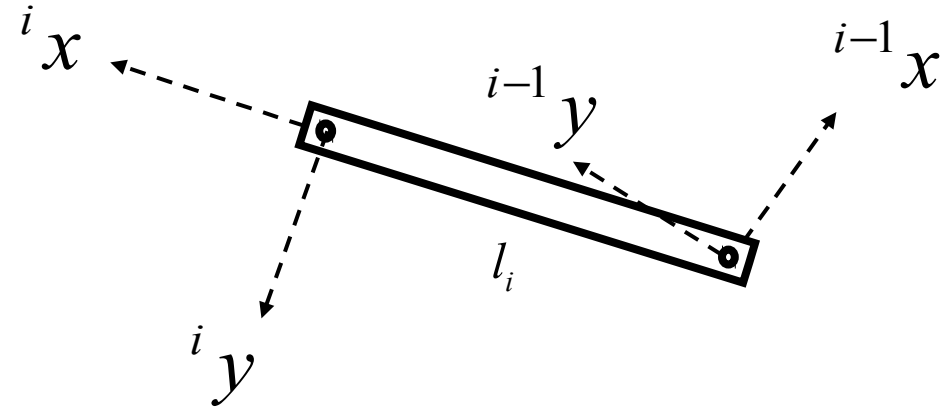
Calculating the Jacobian: Velocity

- The velocity of the end effector caused by motion at the $i-1$ link:

$${}^b \dot{p}_{eff} = \underbrace{{}^b \omega_{i-1} \times {}^b p_{i-1,eff}} + \underbrace{{}^b \dot{p}_{i-1,i}}$$

Velocity at end effector due to rotation at joint $i-1$

Velocity at end effector due to change in length of link $i-1$



Calculating the Jacobian: Velocity

Rotational DOF

- Rotates about ${}^{i-1}z$

$$J_{v_i} = {}^b z_{i-1} \times {}^b p_{i-1,eff}$$

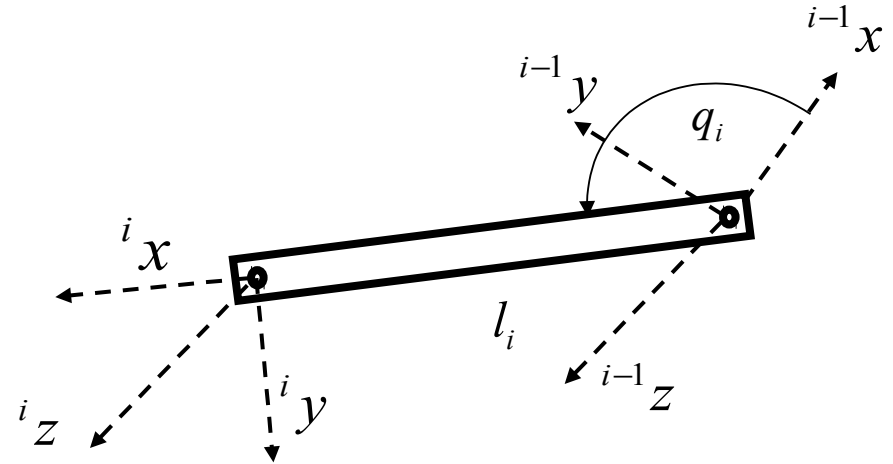
$$J_{v_i} = {}^b z_{i-1} \times \left({}^b p_{eff} - {}^b p_{i-1} \right)$$

Vector from i-1 to the end effector

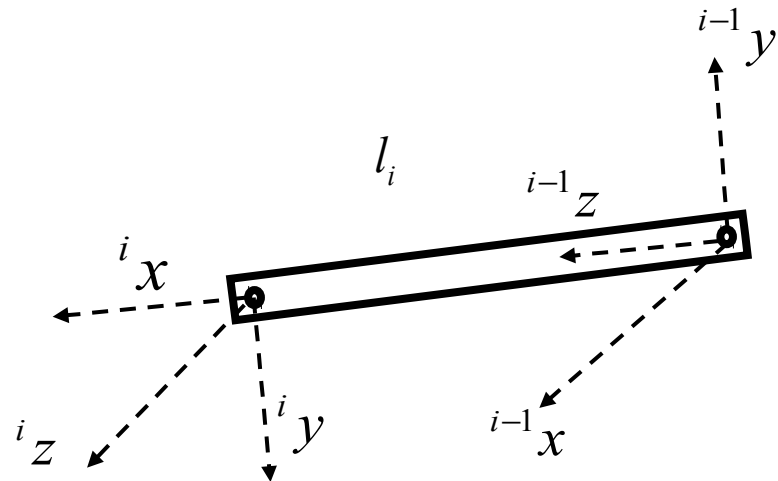
Prismatic DOF

- Translates along ${}^{i-1}z$

$$J_{v_i} = {}^b z_{i-1}$$



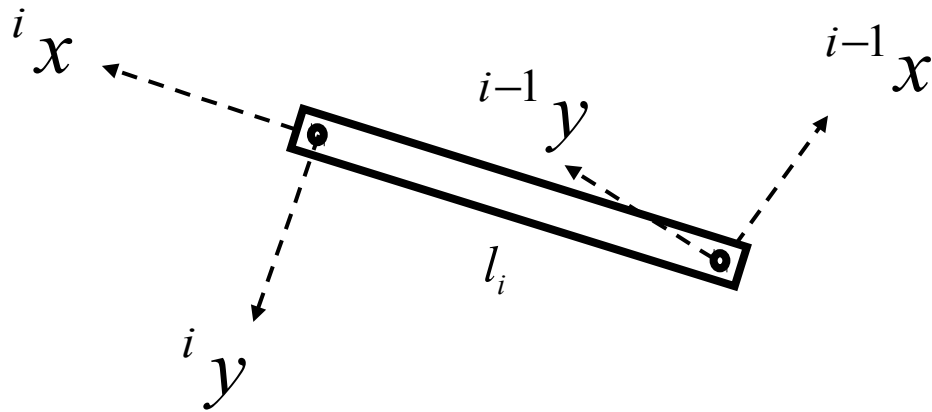
Rotation about ${}^{i-1}z$



Extension/contraction along ${}^{i-1}z$

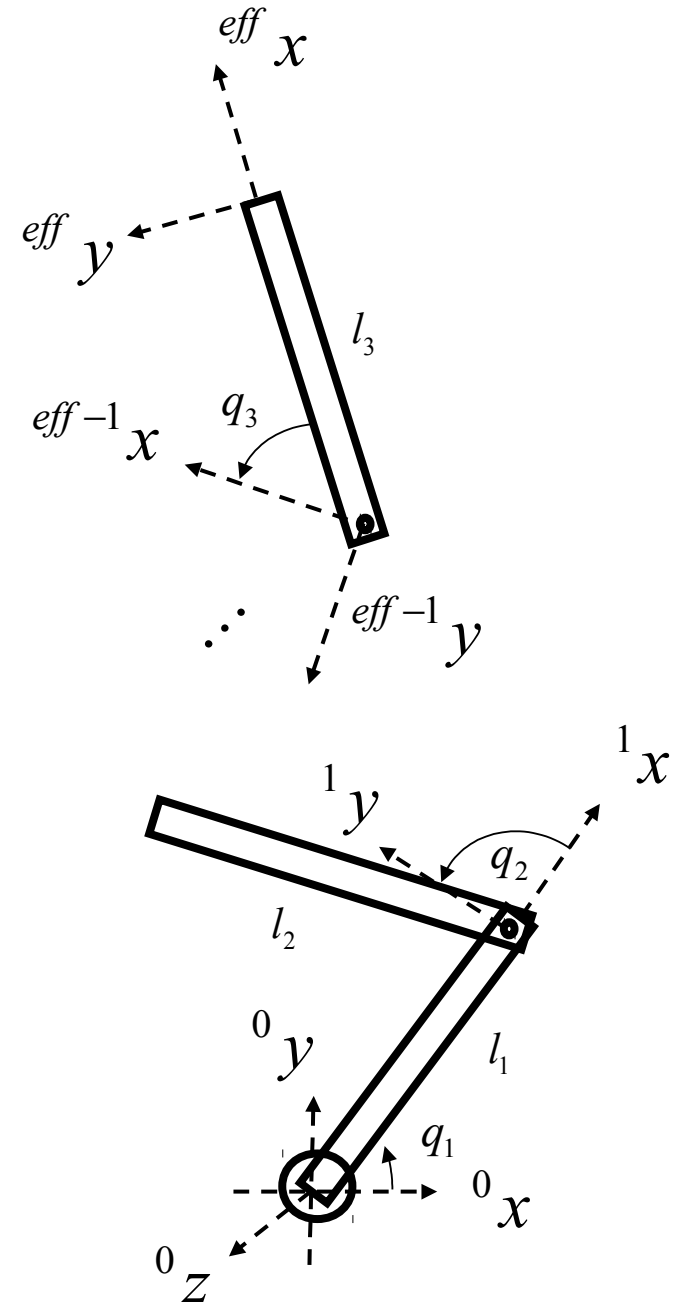
Calculating the Jacobian: Angular Velocity

How does the end effector rotate as the i^{th} link moves?



$${}^b R_{eff} = {}^b R_{i-1} {}^{i-1} R_i {}^i R_{eff}$$

How does ${}^b R_{eff}$ rotate as this rotates?



Calculating the Jacobian: Angular Velocity

$${}^b R_{eff} = {}^b R_{i-1} {}^{i-1} R_i {}^i R_{eff}$$

$${}^b \dot{R}_{eff} = {}^b R_{i-1} {}^{i-1} \dot{R}_i {}^i R_{eff}$$

$$S\left({}^b \omega_{eff}\right) {}^b R_{eff} = {}^b R_{i-1} S\left({}^{i-1} \omega_{i-1,i}\right) {}^{i-1} R_i {}^i R_{eff}$$

$$S\left({}^b \omega_{eff}\right) {}^b R_{eff} = {}^b R_{i-1} S\left({}^{i-1} \omega_{i-1,i}\right) {}^b R_{i-1}^T {}^b R_{i-1} {}^{i-1} R_i {}^i R_{eff}$$

$$S\left({}^b \omega_{eff}\right) {}^b R_{eff} = S\left({}^b R_{i-1} {}^{i-1} \omega_{i-1,i}\right) {}^b R_{i-1} {}^{i-1} R_i {}^i R_{eff}$$

$$S\left({}^b \omega_{eff}\right) {}^b R_{eff} = S\left({}^b \omega_{i-1,i}\right) {}^b R_{eff}$$

$${}^b \omega_{eff} = {}^b \omega_{i-1,i} \longleftarrow \text{Perhaps this was kind of obvious...}$$

Angular velocity caused by rotation of joint $i-1$

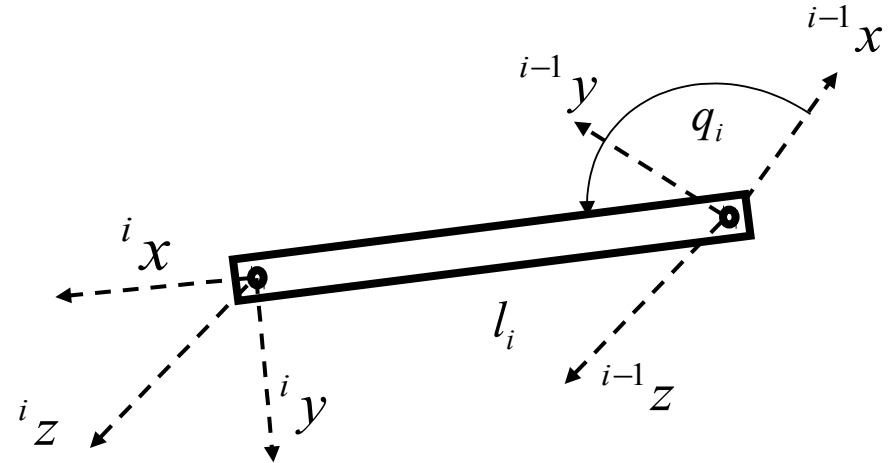
Angular velocity at end effector

Calculating the Jacobian: Velocity

Rotational DOF

- Rotates about ${}^{i-1}z$

$$J_{\omega_i} = {}^b Z_{i-1,i}$$

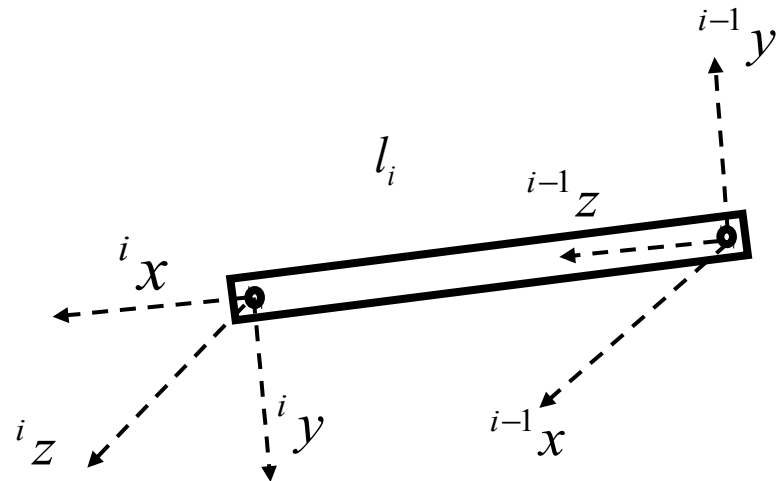


Rotation about ${}^{i-1}z$

Prismatic DOF

- Translates along ${}^{i-1}z$

$$J_{\omega_i} = 0$$



Extension/contraction along ${}^{i-1}z$

Calculating the Jacobian: putting it together

$$J_v = \begin{bmatrix} J_{v_1} & \cdots & J_{v_n} \end{bmatrix}$$

Where

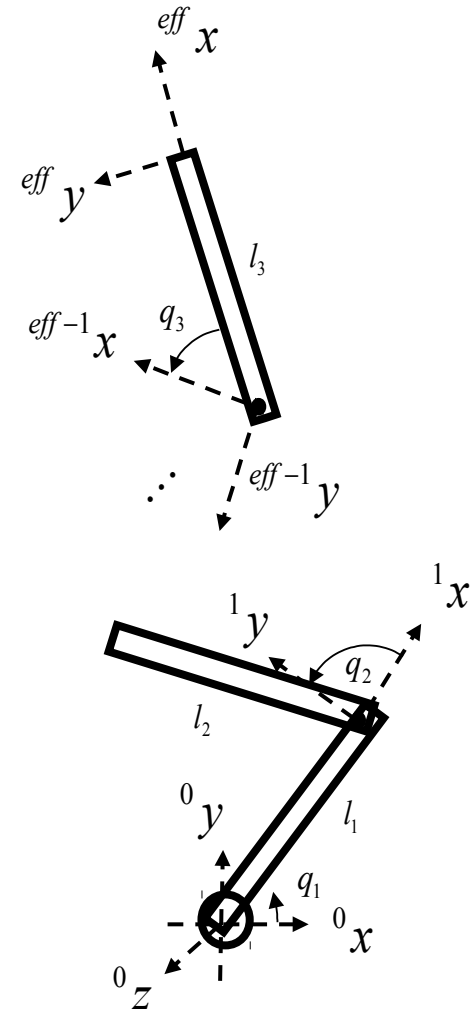
- rotational $J_{v_i} = {}^b Z_{i-1} \times ({}^b p_{eff} - {}^b p_{i-1})$
- prismatic $J_{v_i} = {}^b Z_{i-1}$

$$J_\omega = \begin{bmatrix} J_{\omega_1} & \cdots & J_{\omega_n} \end{bmatrix}$$

Where

- rotational $J_{\omega_i} = {}^b Z_{i-1}$
- prismatic $J_{\omega_i} = 0$

$$J = \begin{bmatrix} J_{v_1} & \cdots & J_{v_n} \\ J_{\omega_1} & \cdots & J_{\omega_n} \end{bmatrix}$$



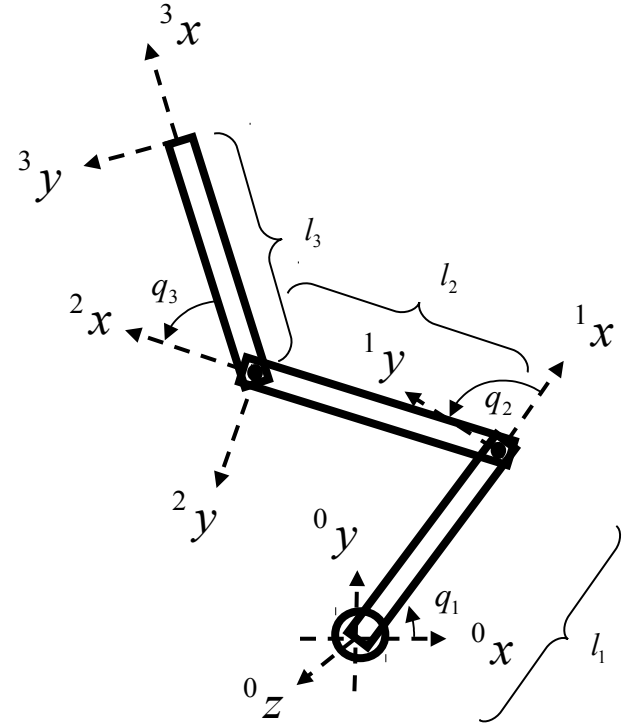
Example 1: calculating the Jacobian

From before:

$${}^0T_1 = \begin{pmatrix} c_{q_1} & -s_{q_1} & 0 & l_1 c_{q_1} \\ s_{q_1} & c_{q_1} & 0 & l_1 s_{q_1} \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{pmatrix} \quad {}^1T_2 = \begin{pmatrix} c_{q_2} & -s_{q_2} & 0 & l_2 c_{q_2} \\ s_{q_2} & c_{q_2} & 0 & l_2 s_{q_2} \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

$${}^2T_3 = \begin{pmatrix} c_{q_3} & -s_{q_3} & 0 & l_3 c_{q_3} \\ s_{q_3} & c_{q_3} & 0 & l_3 s_{q_3} \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

$$J_\omega = \begin{bmatrix} {}^0\hat{z}_0 & {}^0\hat{z}_1 & {}^0\hat{z}_2 \end{bmatrix} = \begin{bmatrix} 0 & 0 & 0 \\ 0 & 0 & 0 \\ 1 & 1 & 1 \end{bmatrix}$$



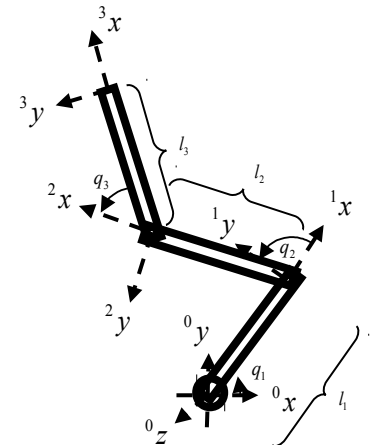
Example 1: calculating the Jacobian

$$J_{v_1} = {}^0\hat{z}_0 \times ({}^0o_3 - {}^0o_0) = \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} \times \left(\begin{bmatrix} l_1 c_1 + l_2 c_{12} + l_3 c_{123} \\ l_1 s_1 + l_2 s_{12} + l_3 s_{123} \\ 0 \end{bmatrix} - \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix} \right) = \begin{bmatrix} -l_1 s_1 - l_2 s_{12} - l_3 s_{123} \\ l_1 c_1 + l_2 c_{12} + l_3 c_{123} \\ 0 \end{bmatrix}$$

$$J_{v_2} = {}^0\hat{z}_1 \times ({}^0o_3 - {}^0o_1) = \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} \times \left(\begin{bmatrix} l_1 c_1 + l_2 c_{12} + l_3 c_{123} \\ l_1 s_1 + l_2 s_{12} + l_3 s_{123} \\ 0 \end{bmatrix} - \begin{bmatrix} l_1 c_1 \\ l_1 s_1 \\ 0 \end{bmatrix} \right) = \begin{bmatrix} -l_2 s_{12} - l_3 s_{123} \\ l_2 c_{12} + l_3 c_{123} \\ 0 \end{bmatrix}$$

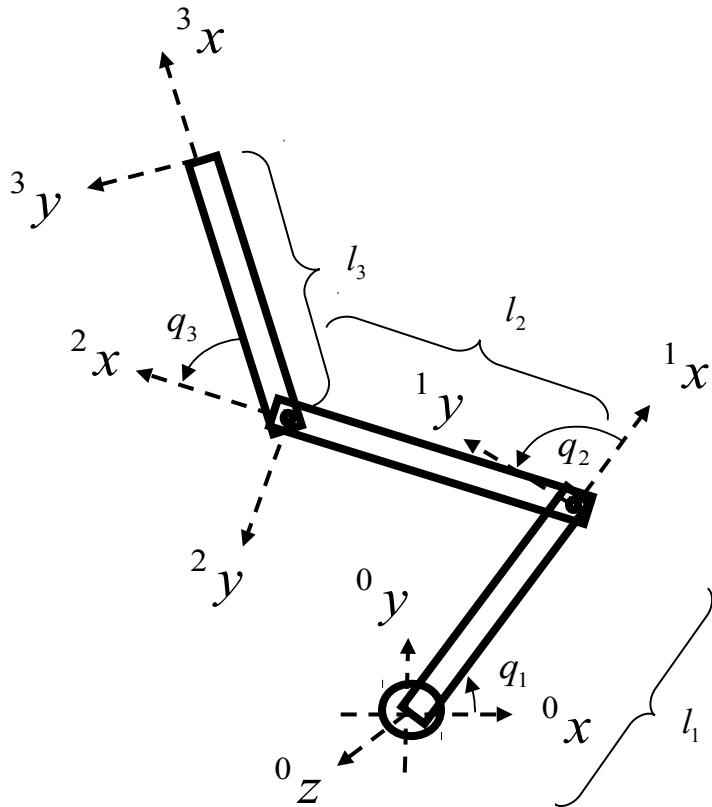
$$J_{v_3} = {}^0\hat{z}_2 \times ({}^0o_3 - {}^0o_2) = \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} \times \left(\begin{bmatrix} l_1 c_1 + l_2 c_{12} + l_3 c_{123} \\ l_1 s_1 + l_2 s_{12} + l_3 s_{123} \\ 0 \end{bmatrix} - \begin{bmatrix} l_1 c_1 + l_2 c_{12} \\ l_1 s_1 + l_2 s_{12} \\ 0 \end{bmatrix} \right) = \begin{bmatrix} -l_3 s_{123} \\ l_3 c_{123} \\ 0 \end{bmatrix}$$

$$J_v = \begin{bmatrix} -l_1 s_1 - l_2 s_{12} - l_3 s_{123} & -l_2 s_{12} - l_3 s_{123} & -l_3 s_{123} \\ l_1 c_1 + l_2 c_{12} + l_3 c_{123} & l_2 c_{12} + l_3 c_{123} & l_3 c_{123} \\ 0 & 0 & 0 \end{bmatrix}$$



Example 1: calculating the Jacobian

$$J = \begin{bmatrix} J_v \\ J_\omega \end{bmatrix} = \begin{bmatrix} -l_1 s_1 - l_2 s_{12} - l_3 s_{123} & -l_2 s_{12} - l_3 s_{123} & -l_3 s_{123} \\ l_1 c_1 + l_2 c_{12} + l_3 c_{123} & l_2 c_{12} + l_3 c_{123} & l_3 c_{123} \\ 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \\ 1 & 1 & 1 \end{bmatrix}$$



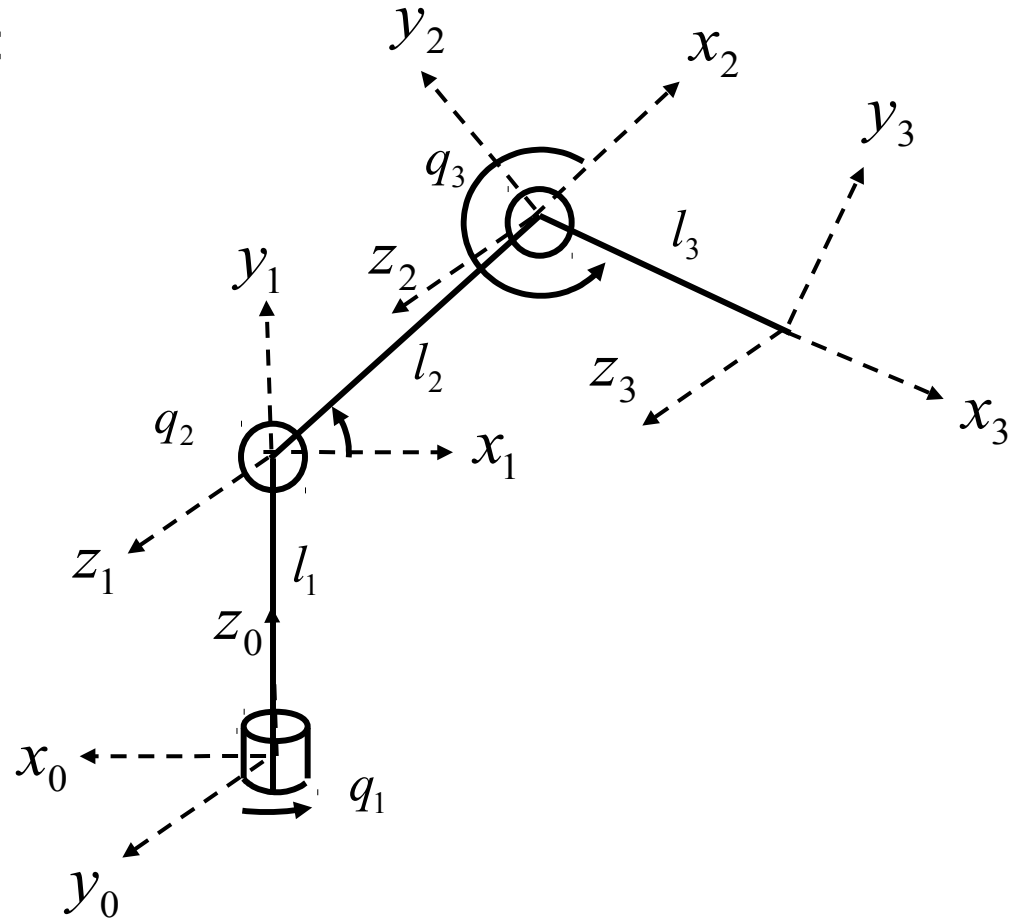
Example 2: calculating the Jacobian

The kinematics of this arm are described by the following:

$${}^0T_1 = \begin{pmatrix} -c_1 & 0 & -s_1 & 0 \\ -s_1 & 0 & c_1 & 0 \\ 0 & 1 & 0 & l_1 \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

$${}^1T_2 = \begin{pmatrix} c_2 & -s_2 & 0 & l_2 c_2 \\ s_2 & c_2 & 0 & l_2 s_2 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{pmatrix}$$

$${}^2T_3 = \begin{pmatrix} c_3 & -s_3 & 0 & l_3 c_3 \\ s_3 & c_3 & 0 & l_3 s_3 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{pmatrix}$$



Example 2: calculating the Jacobian

$${}^b p_0 = \begin{pmatrix} 0 \\ 0 \\ 0 \end{pmatrix}$$

$${}^b z_0 = \begin{pmatrix} 0 \\ 0 \\ 1 \end{pmatrix}$$

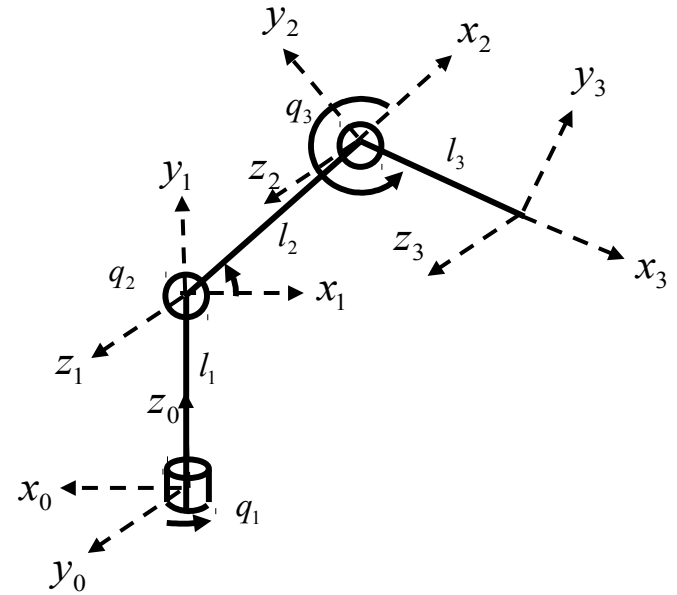
$${}^b p_1 = \begin{pmatrix} 0 \\ 0 \\ l_1 \end{pmatrix}$$

$${}^b z_1 = \begin{pmatrix} -s_1 \\ c_1 \\ 0 \end{pmatrix}$$

$${}^b p_2 = \begin{pmatrix} -l_2 c_1 c_2 \\ -l_2 s_1 c_2 \\ l_2 s_2 + l_1 \end{pmatrix}$$

$${}^b z_2 = \begin{pmatrix} -s_1 \\ c_1 \\ 0 \end{pmatrix}$$

$${}^b p_3 = \begin{pmatrix} -c_1(l_2 c_2 + l_3 c_{23}) \\ -s_1(l_2 c_2 + l_3 c_{23}) \\ l_2 s_2 + l_3 s_{23} + l_1 \end{pmatrix}$$



$$J_{v_1} = {}^b z_0 \times ({}^b p_3 - {}^b p_0)$$

$$J_{v_2} = {}^b z_1 \times ({}^b p_3 - {}^b p_1)$$

$$J_{v_3} = {}^b z_2 \times ({}^b p_3 - {}^b p_2)$$

Example 2: calculating the Jacobian

$$J_{v_1} = \begin{pmatrix} 0 \\ 0 \\ 1 \end{pmatrix} \times \begin{pmatrix} -c_1(l_2c_2 + l_3c_{23}) \\ -s_1(l_2c_2 + l_3c_{23}) \\ l_2s_2 + l_3s_{23} + l_1 \end{pmatrix} = \begin{pmatrix} s_1(l_2c_2 + l_3c_{23}) \\ -c_1(l_2c_2 + l_3c_{23}) \\ 0 \end{pmatrix}$$

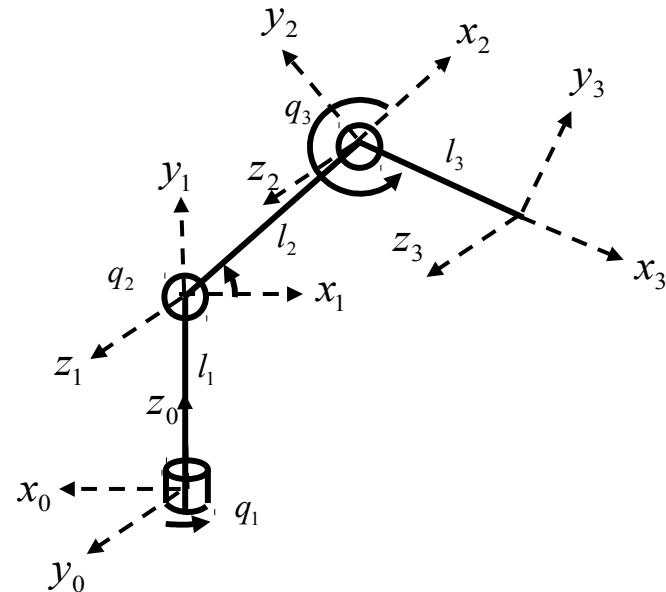
$$J_{\omega_1} = \begin{pmatrix} 0 \\ 0 \\ 1 \end{pmatrix}$$

$$J_{v_2} = \begin{pmatrix} -s_1 \\ c_1 \\ 0 \end{pmatrix} \times \begin{pmatrix} -c_1(l_2c_2 + l_3c_{23}) \\ -s_1(l_2c_2 + l_3c_{23}) \\ l_2s_2 + l_3s_{23} \end{pmatrix} = \begin{pmatrix} c_1(l_2c_2 + l_3c_{23}) \\ s_1(l_2c_2 + l_3c_{23}) \\ l_2c_2 + l_3c_{23} \end{pmatrix}$$

$$J_{\omega_2} = \begin{pmatrix} -s_1 \\ c_1 \\ 0 \end{pmatrix}$$

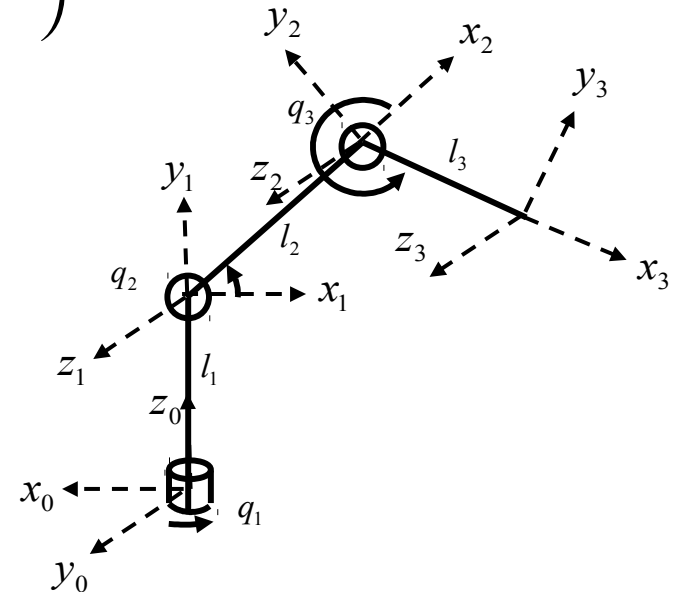
$$J_{\omega_3} = \begin{pmatrix} -s_1 \\ c_1 \\ 0 \end{pmatrix}$$

$$J_{v_3} = \begin{pmatrix} -s_1 \\ c_1 \\ 0 \end{pmatrix} \times \begin{pmatrix} -c_1l_3c_{23} \\ -s_1l_3c_{23} \\ l_3s_{23} \end{pmatrix} = \begin{pmatrix} l_3c_1s_{23} \\ l_3s_1s_{23} \\ l_3c_{23} \end{pmatrix}$$



Example 2: calculating the Jacobian

$$J = \begin{pmatrix} s_1(l_2c_2 + l_3c_{23}) & c_1(l_2c_2 + l_3c_{23}) & l_3c_1s_{23} \\ -c_1(l_2c_2 + l_3c_{23}) & s_1(l_2c_2 + l_3c_{23}) & l_3c_1s_{23} \\ 0 & l_2c_2 + l_3c_{23} & l_3c_{23} \\ 0 & -s_1 & -s_1 \\ 0 & c_1 & c_1 \\ 1 & 0 & 0 \end{pmatrix}$$



Expressing the Jacobian in Different Reference Frames

In the preceeding, the Jacobian has been expressed in the base frame

- It can be expressed in other reference frames using rotation matrices

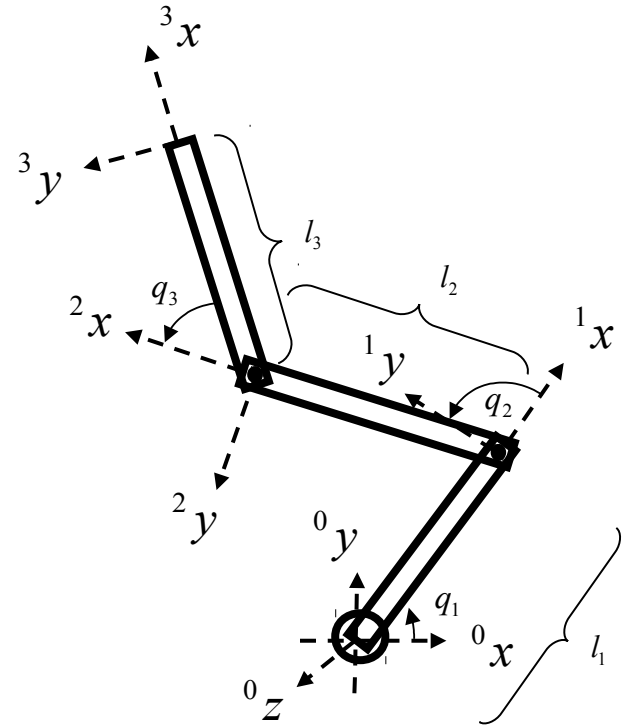
Velocity is transformed from one reference frame to another using:

$${}^k p = {}^k R_b {}^b p$$

$${}^k \dot{p} = {}^k R_b {}^b \dot{p}$$

Therefore, the velocity Jacobian can be transformed using:

$${}^k J_v = {}^k R_b {}^b J_v$$



Expressing the Jacobian in Different Reference Frames

First, let's express angular velocity in a different reference frame:

$${}^b \dot{p} = S({}^b \omega) {}^b p \quad \longleftarrow \text{Def'n of angular velocity}$$

$${}^k R_b {}^b \dot{p} = {}^k R_b S({}^b \omega) {}^b p$$

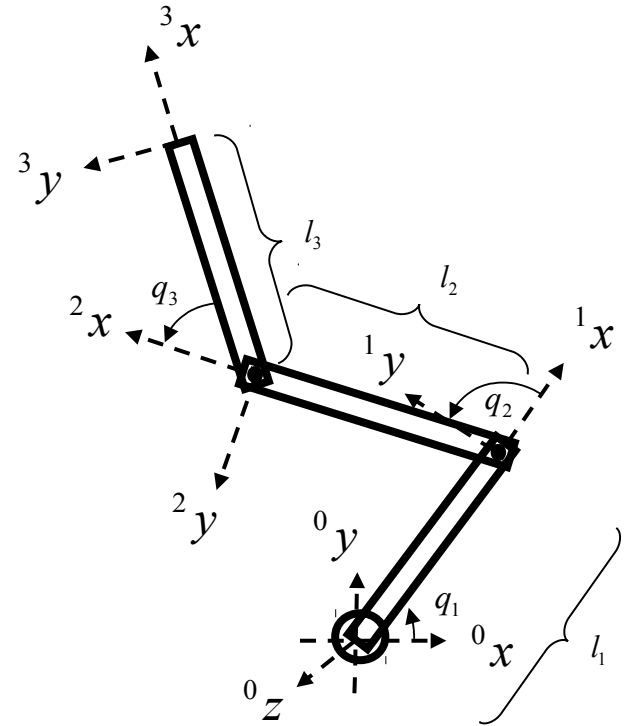
$${}^k \dot{p} = {}^k R_b S({}^b \omega) {}^k R_b^T {}^k p$$

$${}^k \dot{p} = S({}^k R_b {}^b \omega) {}^k p$$

$${}^k \omega = {}^k R_b {}^b \omega \quad \longleftarrow \text{Angular velocity can also be rotated by a rotation matrix}$$

Therefore, the angular velocity Jacobian can be transformed using:

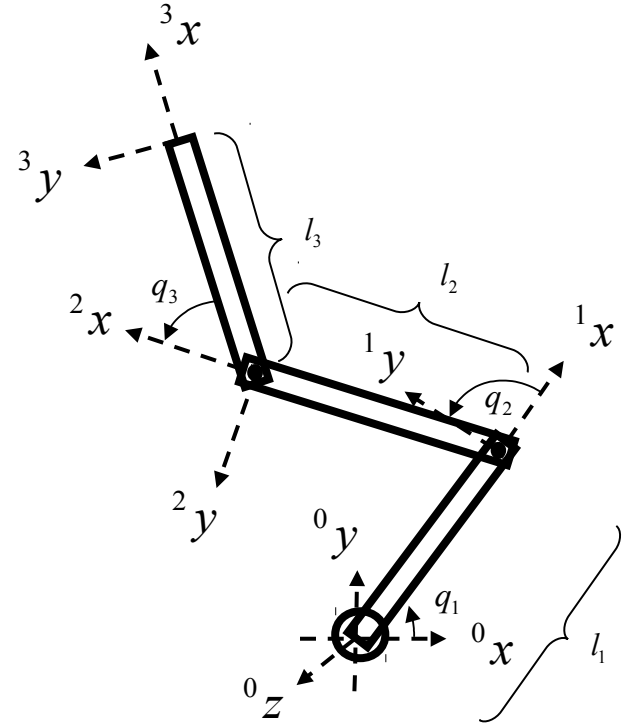
$${}^k J_\omega = {}^k R_b {}^b J_\omega$$



Expressing the Jacobian in Different Reference Frames

Therefore, the full Jacobian is rotated:

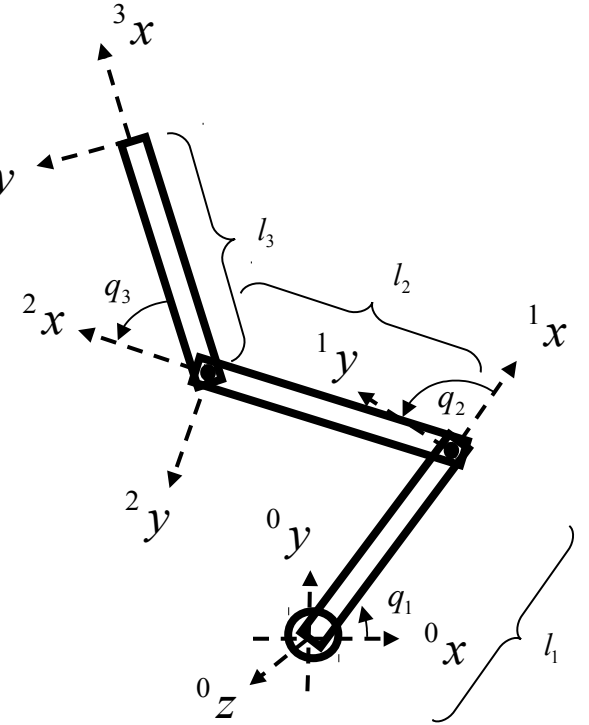
$${}^k J = \begin{pmatrix} {}^k R_b & 0 \\ 0 & {}^k R_b \end{pmatrix} {}^b J$$



Different Jacobian Reference Frames: Example

Express the Jacobian for the three-link arm in the reference frame of the end effector:

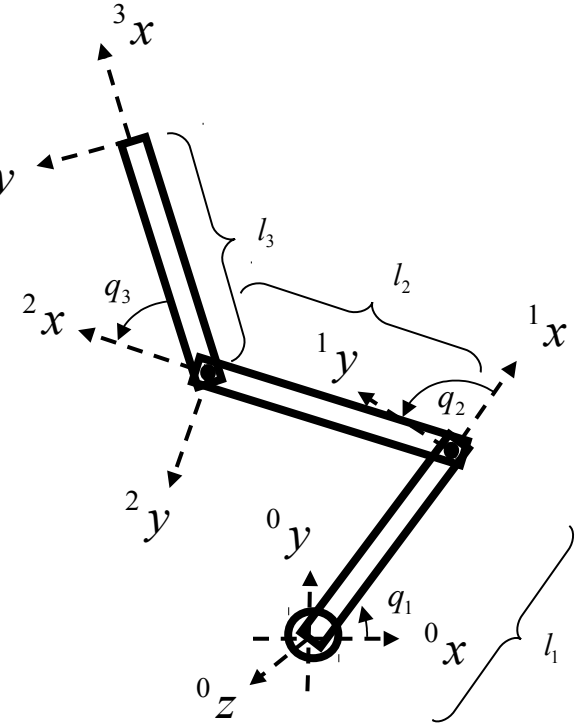
$${}^0R_3 = \begin{pmatrix} c_{123} & -s_{123} & 0 \\ s_{123} & c_{123} & 0 \\ 0 & 0 & 1 \end{pmatrix}$$
$$J = \begin{bmatrix} -l_1s_1 - l_2s_{12} - l_3s_{123} & -l_2s_{12} - l_3s_{123} & -l_3s_{123} \\ l_1c_1 + l_2c_{12} + l_3c_{123} & l_2c_{12} + l_3c_{123} & l_3c_{123} \\ 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \\ 1 & 1 & 1 \end{bmatrix}$$



Different Jacobian Reference Frames: Example

Express the Jacobian for the three-link arm in the reference frame of the end effector:

$${}^0R_3 = \begin{pmatrix} c_{123} & -s_{123} & 0 \\ s_{123} & c_{123} & 0 \\ 0 & 0 & 1 \end{pmatrix}$$



$${}^3J = \begin{pmatrix} c_{123} & s_{123} & 0 & 0 & 0 & 0 \\ -s_{123} & c_{123} & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & c_{123} & s_{123} & 0 \\ 0 & 0 & 0 & -s_{123} & c_{123} & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 \end{pmatrix} \begin{bmatrix} -l_1s_1 - l_2s_{12} - l_3s_{123} & -l_2s_{12} - l_3s_{123} & -l_3s_{123} \\ l_1c_1 + l_2c_{12} + l_3c_{123} & l_2c_{12} + l_3c_{123} & l_3c_{123} \\ 0 & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \\ 1 & 1 & 1 \end{bmatrix}$$